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107	12	COLBERT ELEM.	2701 Plunkett St.	Hollywood	26-00-00	80-09-41	7.52	322.0	10		46 Anixter-Mark	
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117	40	LAKE FOREST ELEM.	3550 S.W. 48th Ave.	Hollywood	25-58-44	80-11-31		339.7	7	- John Ballon Landaus	57 Andrew	P4F-25
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129	47	MIRAMAR ELEM.	6831 S.W. 28th St	Miramar	25-59-15	80-13-30		354.3	8		70 Anixter-Mark	P-25A48G
130 oa 68	81. 61	SHERIDAN PARKIELEMS. ** PERRY, ANNABEL C. ELEM.	2310 NEZOHUTA 6850 S.W. 34th St.	Miramar	25-58-44	# 80-13-48 80-13-32	7.41	355.0	Maria M	HANDARD MARKET STATE OF THE STA	52 Anixter-Mark 11 Anixter-Mark	
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133	8	BOULEVARD HEIGHTS ELEM	A. 7201 Johnson St.	Hollywood	26-01-03	80-14-01	4.73	358.3	8		52 Anixter-Mark	
135	24	FAIRWAY ELEM.	7850 Fairway Blvd.	Miramar	25-58-31	80-14-28 80-14-38	7.65	3.8	5	Market Control of the	30 Anbter-Mark 18 Anixter-Mark	P-25A72G P-25A72G
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139	66	PINES MIDDLE	200 N.W. Douglas Road	Pembroke Pines	28-00-32	80-15-52	5.61	18.5	6	THE RESERVE THE PROPERTY AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON AND A	6 Anixter-Mark	
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143	0	PALM COVE ELEM	11601 S.W. 9th St.	Pembroke Pines	28-00-05	80-18-13		35.9	4	Annual Strange	30 Anixter-Mark	P-25A72G
145	15. 67	COORER GIOCHIGH	9401:String Rocks 5350 S.W. 90th Ave.	Cooper City	26-03-03	80-16-07		40.0	4.5 4	Washington and Street S	6 Conifer	P-25A24 PT-2521
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147	59 4.0 m	PEMBROKE LAKES ELEM.	11251 Taft St.	Pembroke Pines	26-01-28	80-18-20	6.07	45.6	4	15 141 . 911 .	7 Anixter-Mark	P-25A24
149	0	YOUNG WALTER PRESICT EMBASSY CREEK ELEM	ENTERS 90 IN 19 A Zhova (a marsa sa 10905 S.E. Lake Blvd.	Cooper City	26-01-47	80-18-20	5.82	48.2	Mariania 4	profillementation and appropriation of the secretary of the St. Sec. and other	57 Afrixter:Mark 60 Anixter-Mark	P-25A48G P-25A48G
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151 152	28	GRIFFIN ELEM. SILVER RICGE ELEMAN : IN	5050 S.W. 116th Ave.	Cooper City	26-03-21	80-18-11	4.67	63.5	6	49 11 1 1 1	2 Anixter-Mark	P-25A24
153	159	HAWKES BLUFF ELEM.	9100 S.W. Stitt Stand Lace 5900 S.W. 160th Ave.	Fort Lauderdale	28-02-43	80-21-41		70.2	KA A	67 - 196127 67 7	0 ::Anixter:Mark 70 Anixter-Mark	P-25A72G P-25A72G
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155 156	161	TEQUESTA TRACE MIDDLE	1800 Indian Trace CATIONS::1274 Weston Robbins	Fort Lauderdale	26-08-18	80-23-29	9.76	97.4	6	A Section 1	18 Anixter-Mark	P-25A48G
157	0	INDIAN TRACE ELEM	400 Indian Trace	Fort Lauderdale	26-06-54	80-23-31	9.91	90.4 101.6	6	A CONTRACT TO SECURE A CONTRACT OF SECURE AND A SECURE ASSESSMENT OF SECURE	O Conifer Confer Anixter-Mark	PT-2521 P-25A72G
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159	25	FLAMINGO ELEM.		1130 S.W. 133rd Ave		Davie	26-06-17	80-19-32	5.73	103.0	8	35	36	Anixter-Mark	P-25A24
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161 162	163 - 51	CENTRAL PARK ELEM.		777 N. Nob Hill Road 2100 N. And Catherin	all do a consideration	Signal state	20-07-47	BMEDA7219		211110	er Libr	39	40	Jerroid-Taco	EPA-2
163	164	SANDPIPER ELEM.	The second section of the second section is a second section of the section o	3700 Histus Road		Sunrise	26-10-18			147.8	11	68	70	Anixter-Mark	P-25A48G
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165	3 ∞.38 ≈	BAIR MIDDLE HORIZON ELEM		9100 N.W. 21st Mark		Sunrise Sunrise	26-09-03	80-16-15 80-16-09		154.0	, •	41 27	42	Varian ≪ • Anixiai Mark	AE-2 P-25A24
167	0	WESTPINE MIDDLE		9393 N.W. 50th St.		Sunrise	26-11-11			161.8	10	46	48	Anixter-Mark	P-25A48G
168	2.4%	BANYAN ELEM* * 1.4		ero a ni vierboni sie		Sundie L	26-11-07	K. Sandala Market State		Committee of the second second	erio:	49	50	Jefföld-Täčo	EPA-2
169	165	WESTCHESTER ELEM.		12405 Royal Palm Bl		Coral Springs	26-15-35				10	50	52	Andrew	P4F-25
170	<u>166</u> * 168	RIVERSIDE ELEMENTS CORAL SPRINGS ELEM.		11450 RNerside Din 3601 N.W. 110th Ave		Coral Springs	26-16-23			165.1	* ₽ 11	. 68 juli 49		Anixter-Mark Anixter-Mark	P-25A48G P-25A48
172	: 0:a	CABLE TV OF CORALIS		12409 NEATHORES		Coral Springs			14.1.1 1.11.00	0.000	34.3	100	120	Coniter	PT-2521
173	68	PIPER HIGH		8000 N.W. 44th St.		Sunrise	26-10-36			168.0	9	61	63	Anixter-Mark	P-25A48G
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175 # 176	49 - 461706	MIRROR LAKE ELEM. CORAL SPRINGSMIDDE		1200 N.W. /2Nd AVE		Plantation Coral Springs		80-14-41 80-15-53	3.77 -13.88	171.6 172.6		39 49	40 52	Anixter-Mark Anixter-Mark	P-25A72G
177	171	COUNTRY HILLS ELEM.		10550 Westview Driv	/e	Coral Springs	26-17-50	80-15-54	14.65	172.9	12	58	60	Anixter-Mark	P-25A48G
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179		TAMARAC ELEM.		7601 University Dr.		Tamarac	26-12-58				11 - 12:	35 *** 60 ***	37 61 w	Anixter-Mark Anixter-Mark	P-25A48
181	63	PETERS ELEM.		851 N.W. 68th Ave.		Plantation	26-08-04			175.5	7	58	60	Anixter-Mark	P-25A48G
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183	93 44742	VILLAGE ELEM. «PLANTATION MIDDIEW		2100 N.W. 70th Ave.		Sunrise	26-09-09	80-14-25		176.5	8	54 20 3 59	56	Anixter-Mark	P-25A48
185	174	RAMBLEWOOD ELEM.		8950 Shadowwood E	The state of the s	Coral Springs	26-14-51				12	50	60	Coniferation Conference Conferenc	P4F-2521
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187	175	PINEWOOD ELEM. RAMBLEWOOD MIDDLE		1600 S.W. 83rd Ave. 8505 WWATENIE BIV		North Lauderdak				178.7	10	59	60	Anixter-Mark	P-25A24
189	178	CORAL PARK ELEM		8401 Westview Drive		Coral Springs Coral Springs	26-17-59		CONTRACTOR OF THE PARTY	The second second second	// 	51 78	52 52 5 80	Andrew Anixter-Mark	P2F-25 P-25A48G
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page 4 of 4 10/10/2001

Station Information

			Unc	desired		De	esired
Station - Station Name Licensee Channel Groups Call Signs	:	Miami Dade (G KTB8	County	Schools	1		e, FL nty Schools
Coordinates (°,',") - North Latitude West Longitude	:	25 80	46 11	20 20	26 80	5 14	9
Elevations - Ground Tower Height AGL Antenna Radiation Centerline Height AGL Antenna Radiation Centerline Height AMSL	: :	feet 3.0 786.0 780.0 783.0		meters 0.9 239.6 237.7 238.6	feet 9.0 260.0 254.0 263.0		meters 2.7 79.2 77.4 80.2
Antenna - Manufacturer Type or Model # Gain (dBi) Azimuth (°) Beam Tilt (°) Polarization	:	Andrey HMD1 16 295 1.30 H			Andre HMD 14 Omni 0.50 V		
Output Power - Maximum EIRP (dBW) Maximum EIRP (Watts)	:	31.3 1349			28.0 631		

Engineering Declaration

Of Scott D. Ritchie

In response to the Opposition to Petition to Deny filed January 31, 2001, by The School Board of Miami-Dade County, licensee of ITFS station KTB-85, the associated Amendment and Request for Waiver, also filed January 31, 2001, and the Engineering Statements of Ryan Wilhour of Kessler and Gehman and David Mietus of DeLawder Communications, I offer the following information.

On behalf of School Board of Broward County, I have reviewed the above mentioned Opposition, Amendment and Request for Waiver, and all associated engineering. I have performed an independent analysis of the proposed modification of station KTB-85, and I have determined that the proposal will cause substantial interference to the operation of station KTZ-22 licensed to Broward County Schools.

The School Board of Miami-Dade County ("Dade") is the licensee of the F-Group channels (KTB85) in Miami Florida. The School Board of Broward County ("Broward") is the licensee of station KTZ22 (G-Group) in Fort Lauderdale, FL. Dade has requested, by application dated September 15, 1995, to modify station KTB85 to change from the F-Group to the G-Group channels, to change location to downtown Miami, to increase power, to change transmit antenna, and to add digital service. On January 31, 2001, Dade amended their application to increase the mechanical and electrical beam-tilt, and change the digital emission modulation type. Dade's proposed location is 21.8 miles from the Broward transmit location.

In order to facilitate the processing of the modification application of KTB85, for the past six years, representatives from Dade and Bell South (the Miami Wireless Cable Operator) have proposed various solutions to resolve interference between Dade and Broward. These proposals have included the following:

Frequency Offset Mechanical and Electrical Beam Tilt Upgraded Receive Antennas

I have analyzed the proposals, and have determined that no combination of the above mentioned configurations would adequately resolve the interference between the two systems, for three reasons.

1. Dade's application states that KTZ-22 was not eligible for a protected service area ("PSA") at the time of the original application filing (see Interference Study of Kessler & Gehman Exhibit 1 Page 4), and is therefore not eligible for protected service area protection from the amendment. Dade's application requests digital modulation, subject to the Digital Declaratory Ruling in which PSA protection was afforded to all ITFS licensees. Dade's amendment formally requests Digital modulation, including OFDM, qualifying it as a major amendment. For these reasons, Broward is eligible for PSA protection. Dade's modification and amendment cause interference within Broward's PSA.

- 2. Dade's amendment uses a combination of electrical and mechanical beam tilt to reduce signal to Broward's receive sites. Dade did not include an elevation pattern for its proposed antenna, which is not an off the shelf model. While Dade's use of Beam Tilt reduces signal to most of Broward's receive sites, it actually increases signal to four of them. Dade's modification and amendment cause interference to Broward receive sites.
- 3. Dade proposes to upgrade Broward receive sites to reduce interference. In 1994 Broward upgraded its receive antennas to reduce interference from the Miami B-Group. Dade proposes to operate at a higher elevation and higher power than the B-Group, increasing the interference levels. Even with upgraded receive antennas, Dade's modification and amendment will cause interference. Dade's proposal to upgrade receive antennas does not include a proposal to upgrade all current receive sites, only sites registered as of September, 1995, does not propose to modify towers or other structures in order to accommodate the larger receive antennas, does not include a timeline for the upgrades, and does not include a proposal for resolving interference to future sites. As currently proposed, it is unacceptable to Broward for Dade to upgrade Broward's receive antennas, as the upgrades will not resolve all interference issues.

At the time of the Dade proposal, Broward County School District had 189 schools (see Attachment A) receiving educational programming from its ITFS network. Currently, there are 240 schools in service, with additional schools being added continuously. These schools are spread over an area averaging 25 miles wide and 30 miles long encompassing most of Broward County. These Schools each receive locally generated educational programming on eight ITFS channels sixteen and a half (16 ½) hours a day, five days a week. The system operates at 50 watts transmitter power, an omni-directional antenna, and high gain receive antennas designed to maximize signal level and reduce interference. Broward Schools have in the past received interference from Miami ITFS B-Group station WHR866, and have already modified (in 1994) their polarization in order to reduce interference. In addition, Broward has installed high gain, high performance receive antennas to reduce interference. Nevertheless, Broward Schools continue to periodically receive interference from the Miami B-Group station. Broward has constructed towers for each of its schools, on which to install specific receive antennas. Dade's proposal to install new receive antennas is impossible without installing new towers. Furthermore, Dade has not proposed any upgrades to schools that have been added since 1995, nor proposed any solution for resolving interference to future receive sites. That is why Broward must be eligible for PSA protection. For these reasons, it is not an acceptable solution for Dade to upgrade Broward receive antennas.

Dade proposes to operate digital at 50 Watts average transmit power (200 Watts peak power), and an Andrew HMD16HC-W directional cardioid transmit antenna oriented at 295 degrees located 234.4 meters above ground level (770 feet). They propose to utilize -1.3 degrees of electrical beam tilt and -0.8 degrees of mechanical beam tilt at an azimuth of 355.0 degrees. Peak EiRP would be 31.3 dBW.

Dade proposed to Broward to utilize frequency offset, yet they propose to utilize digital transmissions. There will be no benefit from frequency offset when digital transmission is used, therefore no decrease in required Desired to Undesired (D/U) signal level ratio is acceptable.

Dade proposes to use an antenna with -1.3 degrees of electrical beam tilt, yet there is no antenna elevation pattern included in their application. According to representatives from Andrew Corporation, and according to Andrew Catalog Number 38, the elevation pattern for antenna model HMD16HW-W is based on -0.5 degrees of tilt. The elevation pattern for HMD16HW-W-1.5 which is the same antenna with -1.5 degrees of electrical tilt, is available from Andrew, but differs from the -0.5 degree tilt pattern. In other words, you cannot just shift the standard elevation pattern to change the tilt. In order to get the pattern for HMD16HW-W-1.3, Andrew would have to generate a new elevation pattern. Dade has not submitted such a pattern with its application, therefore there is no way to determine the actual decrease in signal level due to beam tilt toward Broward receive sites. Since the antenna is not an off the shelf model, the predicted decrease in signal level due to mechanical and electrical tilt was not used in the attached engineering analysis. Rather, the study assumes peak signal in the vertical plane, and uses the standard horizontal radiation pattern for the proposed antenna.

An interference analysis using such parameters is attached. Attachment B is a receive site interference analysis. The parameters used are those specified in the Dade amendment. It demonstrates that out of the 189 receive sites studied, 88 (identified with an asterisk), will have a D/U ratio of less than the required 45 dB, when the existing receive antenna pattern is used. It should be noted that not every existing receive antenna has an available radiation pattern. Some of the antennas in use are no longer being manufactured, and the antenna radiation pattern is not available. Those with an available receive antenna radiation pattern are in Bold. The receive antenna in use at each school is identified on Attachment A. The interference analysis of Ryan Wilhour used an Andrew antenna pattern for some sites that is not the receive antenna in use (see Interference Study of Kessler & Gehman Exhibit 2 Page 2A). In cases where the existing antenna pattern was not available, the FCC standard receive antenna pattern was assumed. Additionally, Attachment B shows the D/U ratio using just the FCC reference receive antenna for all receive sites. In this analysis, 97 receive locations have a D/U ration less than the required 45 dB. Attachment C is a map showing the Miami and Broward transmit locations, the 189 BECON receive locations (using the FCC reference receive antenna), and the 45 dB D/U contour. The map shows that approximately half of the BECON receive sites are outside the contour, and will therefore receive interference. The map also shows that a majority of BECONs 35 mile protected service area ("PSA") will receive interference. Finally, the last part of Attachment B is a study showing the interference level to all 189 schools using the proposed antenna upgrade identified in the Dade amendment. It demonstrates that even if all schools were to use the proposed high performance antenna, there would still be interference to 27 schools.

The Dade Amendment increases Dade's signal level to 4 of the Broward Schools through its use of mechanical and electrical Beam Tilt. In addition, the Dade Amendment increases signal level to an additional 4 hypothetical sites by more than 6 dB. This is shown on Attachment D. The request also asks for Digital modulation not requested in the original application (see Dade amendment application, FCC Form 330, Page 9). These changes qualify the amendment as a major amendment. As a result, Broward is entitled to PSA protection.

In conclusion, it is without reason to expect that two co-channel ITFS Systems can coexist 22 miles apart from one another. That is the situation in Dade and Broward Counties. Dade has asked Broward to accept interference to almost half of its receive sites. The attached

interference analyses demonstrate that even with the upgraded receive antennae, there will be harmful interference to Broward Schools.

I hereby certify under penalty of perjury that the forgoing is true and correct to the best of my knowledge, that I am the engineer responsible for the research and preparation of the above information, that I am familiar with Part 21 and 74 of the Commission's rules, and that I am technically qualified to perform this study.

Date: 10/24/01

Scott D. Ritchie

Senior Engineer

Cornerstone Wireless Communications

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7	117	CORAL SPRINGS HIGH	7201 W. Sample Road	Coral Springs	26-16-23				111	2 64	Andrew	P4F-25
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33	133	DEERFIELD PARK ELEM.	627 S.W. 2nd Ave.	Deerfield Beach	26-18-31				16 4		Andrew	P4F-25
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87 0	WRIGHT, K.C. ADMIN. BLDG.	600 S.E. 3rd Avenue	Fort Lauderdale	26-06-51	80-08-24		251.8		176 1	78	Anixter-Mark	P-25A48G
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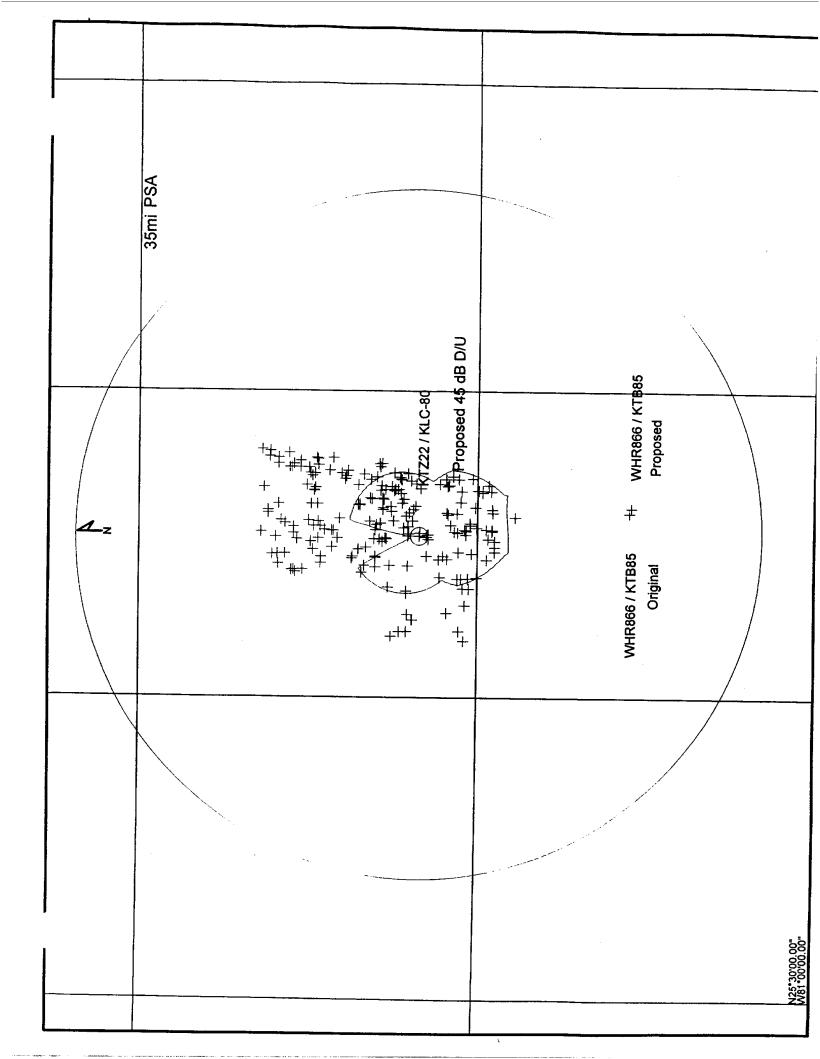
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NO. NO.	SCHOOL	ADDRESS	CITY	LAT	LONG D			3673 L. J.	GHT AGL	MANUFACTURE	R MODEL
106 35		3501 Tan St	· Hothwood &	2,000	=:80-10-50×±		A	32	34	Anixter-Mark	
107 12	COLBERT ELEM.	2701 Plunkett St.	Hollywood	26-00-00	80-09-41 7		10	43	46	Anixter-Mark	P-25A48 P-25A72G
108 101	and the second s	1411 S. 28th Ave.	Hollywood		80-09-42 , 7		and the same of th	41.00 (3)	44	Anixter-Mark	P-25A72G
109 85	STIRLING ELEM	5500 Stirling Road	Hollywood	26-02-37		66 323.1	5	58	60	Anixter-Mark	P-25A48G
110 29		. (20.5202411.Ave.	Hallandale		80-09-10		W.40	68	70	Anixter-Mark	P-25A48G
111 30	HALLANDALE HIGH	720 N.W. 9th Ave.	Hallandale	25-59-35	80-09-43 7		10	54	57	Anixter-Mark	P-25A72G
1.12 / 157	SOUTH AREA ALTERNATIVE CTR-	*#CIFO NO VETER Court	Hallendale	25-59-35	* 80-09-53 ₋ 7	76 - 325.4	10:	56	58	Anixter-Mark	P-25A48
113 31	HALLANDALE ADULT/COMM CTR.	1000 S.W. 3rd St.	Hallandale	25-58-49	80-09-47 8	55 328.2	11	55	57	Jerrold-Taco	EPA-4
114 80	SHERIDAN HILLS, ELEM.	SUULATIONAS SU, 10 11 11 11	Hollywood	and the second of the second o	180-11-08L A	andrough Philippi, my chart actual under und grant and g	AND RESIDENCE CONTRACTOR OF STATE OF ST	58	60	Anixter-Mark	A
115 100	ORANGE BROOK ELEM.	715 S. 46th Ave.	Hollywood	26-00-13	80-11-20 6	transport of the second of the second	TO ARREST AND ADDRESS OF A COMMON COM	58	60	Anixter-Mark	P-25A48
116 109		SHOOTHESTERMENSULF			80-12-79: 4	CONTRACTOR OF THE PROPERTY OF	BOY DON'T CHARLES STATES AND A VANCOUS CONTRACTOR	62	64	Anixter-Mark	P-25A48
117 40	LAKE FOREST ELEM.	3550 S.W. 48th Ave.	Hollywood	25-58-44	80-11-31 7.			55	57	Andrew	P4F-25
118 108 119 95	A QUEST CENTER WITH THE WATER TO THE WATER T	3601 S.W. 56th Ave.	Hollywood	26-02-24 25-58-40	80-13-04 2 80-11-51 7			35 64	36 66	Andrews	P2F-25 P4F-25
1.0	WESTHOLLYWOOD ELEM: NOW	and the second s		1.1.140 1.1.40	· 80-12-525	and the second s		T	- 00 ×70 × 100 ×	Andrew Anoder-Mark	
121 102		6501 Hollywood Blvd.	Hollywood	26-00-38	80-13-04 5		Chandrate Montale Management and the control of the	28	31	Anixter-Mark	P-25A72G
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	T.C.L. of SOUTH FLORIDA CABLE	TEST NATURAL N			60-12-15: 9			00	150	Andrews	
123 0	NOVA EISENHOWER ELEM	6501 S.W. 39th St.	Davie	26-04-22	80-13-59 0.			59	60	Anixter-Mark	P-25A24
124510 60	PEMBROKE PINES ELEMI	· · · · · · · · · · · · · · · · · · ·	Pembroka Pines	26-00-06	::80-13-19::45	88 351.5	7 4	23.	25	Anixter-Mark	P-25A48
125 1	APOLLO MIDDLE	6800 Arthur St.	Hollywood	26-01-10	80-13-32 4.	63 352.1	8	56	57	Conifer	PT-2521
126 54	and the property of the first of the following person and the first of	3821 Dayie Hoad	E Daywar	26-04-27	80-14-02 0	81 4 (352.6 _{87.4}	ég, Brezer	59	¢60. + : : . ×	:Anixter-Mark	P-25A24
127 0	DRIFTWOOD MIDDLE	2751 N.W. 70th Terr.	Hollywood	26-02-04	80-13-44 3.			39	40	Andrew	P2F-25
	HOLLYWOOD PARKELEM	901 N. 69th Ways out	G Hollywood		(,80-13-39) " 4.	The second secon	Margane Before destination and an inches and	68	70	Anbter-Mark	P-25A48G
129 47	MIRAMAR ELEM.	6831 S.W. 26th St.	Miramar	25-59-15	80-13-30 6.			68	70	Anixter-Mark	P-25A48G
13081 131 61	SHERIDAN PARK ELEM, IV. PERRY, ANNABEL C. ELEM.	2310 N.770th Tark is the way	NAME AND ADDRESS OF A PARTY OF A		780-13-46-13			51 .*	52	Anbder-Mark	
13221 1 62	CONTRACTOR OF THE CONTRACTOR O	6850 S.W. 34th St	Miramar Miramat	25-58-44	80-13-32 7. 80-13-39 7			39	41	Anixter-Mark	P-25A48G
133 8	BOULEVARD HEIGHTS ELEM.	7201 Johnson St.	Hollywood	26-01-03	80-14-01 4.		BECOMMENDATION & WORKSON SOLVED 1 14000 5-	58 51	70 · · · · · · · · · · · · · · · · · · ·	Anixter-Mark	P-25A48G P-25A24
134 91	the country of the co	7797 W/LeSale Blvda			80-14-25-6			7 7	52 .80	Anixter-Mark Anixter-Mark	P-25A72G
135 24	FAIRWAY ELEM.	7850 Fairway Blvd.	Miramar	25-58-31	80-14-38 7.		AND DESCRIPTION OF THE PROPERTY OF THE PROPERT	45	48	Anixter-Mark	P-25A72G
136	WHISPERING PINES SCHOOL	3809 S.W/ 896 AVekt	sisMiramer «		6.80-15-14×77	The second secon	Manager M. J	5 8	70	Another-Mark	P-25A48G
137 55	NOVA HIGH	3600 College Ave.	Davie	26-04-32	80-14-15 0.	Carlo Car	CONTRACTOR OF THE PROPERTY OF THE PERSON OF	59	60	Anixter-Mark	P-25A24
	MIRAMAR HIGH	3501.S.W. Egitt Ave. 1	#Miceman	25-58-31	80-15-41-7,	793-16118-22	1.7	34	37	Anoder-Mark	P-25A72G
139 66	PINES MIDDLE	200 N.W. Douglas Road	Pembroke Pines	26-00-32	80-15-52 5.			35	36	Anixter-Mark	P-25A24
	SEA CASTLE ELEM.	9600 Mramm Blvd 1	the time and proceedings of the second secon		. 80-16-28-17.	-consect disable additions because a second backers of balds of \$1.	an extension of second and obligation and the contract of the	52 066 differences	60 3 11	- Anixler-Mark.	
141 18	DAVIE ELEM.	7025 S.W. 39th St.	Davie	26-04-22	80-14-27 0.			19	20	Conifer	PT-2521
143 0	PASADENA LAKES ELEM. PALM COVE ELEM	11601 S.W. 9th St.	to a medical professional and definition of the property of the second control of the property of the second control of the second c		80-15 -4 5.64.		######################################	38 - 1	dispersion of the standard of the A	Anixter Mark	Con Change Congression of the Property of
144 541 - 45		2401 Shring Road ***	Pembroke Pines	26-00-05	80-18-13 7. 80-18-25 3			7 7 ¥ m anatai©is€aassa	80	Anixter-Mark	P-25A72G
145 67	PIONEER MIDDLE	5350 S.W. 90th Ave.	Cooper City	26-03-03	80-16-07 3.			15 15	46	Anixter-Mark	P-25A24 PT-2521
» 146 65				26-00-51			en	•0 S2	46 55	Conifer Anixter-Mark	
147 59	PEMBROKE LAKES ELEM.	11251 Taft St.	Pembroke Pines	26-01-28	80-18-20 6.		CONTRACTOR OF STATE O	36	37	Anixter-Mark	P-25A24
148		901209/2429m Aveder & 1		26-00-45	-80/10/18 /27 /	Water Common Court (MANAGED CO. CRISTING St.)		25 to 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	67	Anixin Alarka	P-25A48G
149 0	EMBASSY CREEK ELEM	10905 S.E. Lake Blvd.	Cooper City	26-01-47	80-18-20 5.	ALCOHOLD STATE OF THE PARTY OF	and the property of the contract of the contra	58	60	Anixter-Mark	P-25A48G
150 14	COOPER CITY ELEM	5080-S:W: 925d AV6		26-03-26	80-16-26: 3		Contract of the Contract of th	15	A6	Andrews	P2F-25
151 28	GRIFFIN ELEM.	5050 S.W. 116th Ave.	Cooper City	26-03-21	80-18-11 4.	63.5	MARKANDA KIRL LUMORIS - 57, 1 - 10, NORMAN	11	42	Anixter-Mark	P-25A24
152 - 162	A CONTROL TO APPROXICE CONTROL	Priod S.W. 136th St. 146	N/Dayldhin	26-04-30	80-16-07 2	181 (189 44)	44.6	37 *** *****	70 🖫 🐃	Anixter-Marks	P-25A72G
153 159	HAWKES BLUFF ELEM.	5900 S.W. 160th Ave.	Fort Lauderdale	26-02-43	80-21-41 8.	30 70.2	6 6	37	70	Anixter-Mark	P-25A72G
154. 160.		2300 Country leig Road (and	Minister of Land St. Market St. Committee of St. Committe	26-05-45	40-22-21×-8			to the describer and a second	70	Anixier-Mark*	P-25A48G
155 161 156 0**	TEQUESTA TRACE MIDDLE	1800 Indian Trace	Fort Lauderdale	26-06-16	80-23-29 9.			16	48	Anixter-Mark	P-25A48G
156 0 157 0	 GULF & PACIFIC COMMUNICATIONS INDIAN TRACE ELEM 	5 1274 Weston Rd 400 Indian Trace	Westori Fort Lauderdale	26-06-14 26-06-54	80-24-49Aug		cuito conditata la Refusa	Manager and the Control of the Contr	70	Confer	PT-2521
	WESTERN HIGH	1200 S.W. (136th Ave.		26-06-54 26-06-17	80-23-31 9.5	91 101.6 95 102.5		7 	60	Anixter-Mark	P-25A72G
V	A CONTRACTOR OF THE PARTY OF TH	INA NATIONAL TANKS	OIL LOUIS UNION	FA-AD-TV	ON-18-40 OF	IV.C.	8 8	7	68	Anixter-Mark	P-25A24

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OLD		.%		141							
NEW FCC FCC		Carte Control			2.0		COLUMN GRO	DAND	STRUCTURE	Q. Carrie	e a serie
NO. NO.	SCHOOL	ADDRESS.	CITY	ELECTIV	LONG	DIST	LAZ EL	EV. I	RCAGL HEIGHT AGL	MANUFACTURER	MODEL
159 25	FLAMINGO ELEM.	1130 S.W. 133rd Ave.	Davie	26-06-17	80-19-32	5.73	103.0	8	35 36	Anixter-Mark	P-25A24
140 t 0	SAWGRASS ELEM.	THE PROPERTY OF THE PROPERTY O	Sunnse	- 7 processors depth of the annual accountage of	Ann. Nicolegistics.photographics.nach.com	Control to A State of the Control	A121/2	\$	58 60	-Antxter-Mark	
161 163	CENTRAL PARK ELEM.	777 N. Nob Hill Road	Plantation	26-07-47	80-17-01	4.22	135.3	8	57 60	Anixter-Mark	P-25A72G
162 51 163 164	NOB HILL ELEM SANDPIPER ELEM.	2100 N.W. 104th Ave. 3700 Hiatus Road	Sunrise Sunrise	26-09-03 26-10-18	80-17-12 80-17-44	5.40 6.96	144.6 (147.8 1	940.	39 40 68 70	Jerrold-Taco	P-25A48G
163 164 1. 2164 0	WELLERY ELEM.		Sunrise Sunrise				147.8 (151.9/2.7-1	•	68 70 68 70	Anixter-Mark Anixtet-Mark	P-25A48G
165 3	BAIR MIDDLE	9100 N.W. 21st Manor	Sunrise	26-09-03	80-16-15		154.0 7	7	41 42	Varian	AE-2
i-166 : 38 :	HORIZON ELEM.	MANUTER CHARGE ROAD	Sunnise	26-09-04	80-16-09	4.93	.455.1	7	37 38	Anixter-Mark	P-25A24
167 0	WESTPINE MIDDLE	9393 N.W. 50th St.	Sunrise	26-11-11	80-16-20			0	46 48	Anixter-Mark	P-25A48G
4: 168 - , 4	BANYAN ELEMENT AND A STATE		Sundse	CA THE SAME OF TAXABLE OF THE SAME	60-10-08	CONTRACTOR NAME OF STREET	State of American State of the	et and a second	49 50	. Jenoid Taco:	EPA-2
169 165	WESTCHESTER ELEM.	12405 Royal Palm Blvd.	Coral Springs	26-15-35	80-17-26			0	50 52 68 70	Andrew	P4F-25
170 - 166 171 168	RIVERSIDE ELEMA CORAL SPRINGS ELEM	3601 N.W. 110th Ave.	Coral Springs Coral Springs	26-16-23	80-17-27	CONTRACTOR CONTRACTOR CONTRACTOR	165.1 1) 1	49 51	Anixter Mark Anixter-Mark	P-25A48G P-25A48
×331720	CABLE TV ORGONAL SPRINGS	ATZAGONI WEST STA	Cont Springs		×80-17-20				100 - 420	Confe	PT-2521
173 68	PIPER HIGH	8000 N.W. 44th St.	Sunrise	26-10-36	BOOK STATE OF THE PARTY OF THE	6.37	168.0 9	Married School	61 63	Anixter-Mark	P-25A48G
174400 167		Berry Committee (Donath Care and Artist	The second secon				Piesy 1	Q	52 53	Arikfer-Wark	. P-25A24
175 49	MIRROR LAKE ELEM.	1200 N.W. 72nd Ave.	Plantation	26-08-25	80-14-41		171.6 8	3	39 40	Anixter-Mark	P-25A24
176 170	CORAL SPRINGS MIDDLE COUNTRY HILLS ELEM.	10550 Westview Drive	CONTRACTOR SECTION AND ADMINISTRATION OF THE PROPERTY OF THE P	26-17-50	80-15-53 80-15-54		172.8 % 1		49 62	Another Mark	P-25A72G
¥ 178 169	STONEMAN DOUGLAS HIGH		Coral Springs Partiend	20-17-50 x26-18-16					58 60 85 87	Anixter-Mark	P-25A48G
179 172	TAMARAC ELEM.	7601 University Dr.	Tamarac	26-12-58	80-15-13	CANADAMAN COME POSSESSAM	Same and the same	2001/1850/1871 (1781/1781)	35 37	Anixter-Mark	P-25A48
###18Q#### 173	MAPLEWOOD ELEM, 444 444		Coral Springs	204 4013	#80x164251	10.00	1173.1-1-1	2	B0 61	· Antheir Mark	P-25A24
181 63	PETERS ELEM.	851 N.W. 68th Ave.	Plantation	26-08-04	80-14-24	3.34	175.5 7	;	58 60	Anixter-Mark	P-25A48G
70	PLANTATION HIGH	Mark Control of the C	(Plantifled)	AND THE RESIDENCE AND THE ARREST OF THE PARTY OF THE PART	ACCUSANCE OF THE PROPERTY OF T	A STATE OF THE PARTY OF THE PAR	#75'e : 1 - 8	Pacinita num viantitikkes	35	Anotter Mark	P-25A48
183 93	VILLAGE ELEM. PLANTATION MIDDLE	2100 N.W. 70th Ave.	Sunrise Plantation	26-09-09		4.58	176.5 8	•	54 56	Anixter-Mark	P-25A48
185 174	RAMBLEWOOD ELEM.	8950 Shadowwood Blvd.	Coral Springs	26-14-51	80-14-41			search on the fact of the fact	59 50 50 52	Coniter Andrew	PT-2521 P4F-25
186			Coral Screens				478.6		44 47	Anoxier Mark	P-25A72G
187 175	PINEWOOD ELEM.	1600 S.W. 83rd Ave.	North Lauderdale\	26-12-28	80-14-20	CHARLEST HAT PART PARTY CONT.	178,7 10	echebbilitabilitati an artiri i	59 60	Anixter-Mark	P-25A24
488 . 177	RAMBLEWOOD MIDDLE		us to 1654 Distribution consequence constitution and significant statements and significant statements and second	: 26-14 <u>/</u> 103	THE RESIDENCE AND ADDRESS OF THE PERSON OF T	WALKER WITH THE	ESTATEMENT OF THE PROPERTY OF THE PARTY.	farri e	51 ·	Andrew	P2F-25
189 178	CORAL PARK ELEM.	8401 Westview Drive	Coral Springs	26-17-59	80-14-14				78 80	Anixter-Mark	P-25A48G
FUTURE	FORT LAUDERDALE POLICE DEPT. EE MIDDLE SCHOOL	Sample Rd. @ NW 124th Ave		26-07-16 26-16-15	80-17-41	THE RESERVE OF THE PARTY OF THE	2628 5 163.9 0	Para de la constantina della c	100 . 200	Andrew	P4F-25
JEUTURE * 2	SILVER TRAIL MIDDLE	STATISTIC ON MERCATO AVE.		28-01/394			87.5		\A\A\A\A\A\A\A\A\A\A\A\A\A\A\A\A\A\A\A	Andrew Andrewi-	FUTURE
FUTURE	INDIAN RIDGE MIDDLE	Nob Hill Rd. @ SW 14th St	Davie	26-06-11	80-17-04	A SECULAR SECURITIES SECURIT	111.3 0	entation in the end fed ease.	0 0	Andrew	FUTURE
FUTURE	CHAPELITRAIDELEMBANA LA CA	LITATISTICO NIVETPENDAVELLE	Pembroke Pines.	-26-01 5 3 5	e02428	14,50	e 67,1 ₅₀ × +0	1	0 84.	AnixtenMark:	P-25A48G
FUTURE	EAGLE TRACE ELEM	Indian Trace @ I-595	Weston	26-07-37		10.58	105.6 0		0 64	Anixter-Mark	P-25A48G
FUTURE	I-91 SILVER PALMS ELEM	Colorador de la marca de la colorada de la colorad	Cocoput Creek	A NOT THE REPORT OF THE PROPERTY OF THE PROPER	1000 にできない取り がませたが になった。	ANALYSIS SANS	188.6	Page 10 State of the State of	, Q	Arkitewa.	FUTURE
FUTURE		I-75 @ Pines Blvd Coral Spr. Dr. @ W. View	Pembroke Pines Const Springs	26-01-07	80-20-55		56.7 0 4 68.9 0		0 0	Andrew Andrew	FUTURE
FUTURE	FLANAGAN HIGH SCHOOL	12800 Taft Street	Pembroke Pines		80-19-17		50.4 0	\$600 per production (\$1000)	0 0	Andrew	FUTURE
FUTURE	TECHNICAL SUPPORT SERVICES								30 30		FUTURE

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Total	Š	Ratio	dВ	46.7	26.6		25.5	39.5		4.00	202	ניים ב	3/./	29.8	42.2		28.2	40.6		27.9	40.4		32.0	33.4		29.0	40.1	31.3	26.36	30.3	40.1	31.9	36.9		29.7	39.7		41.4	38.2	603	29.3
	_	"U	dВ	-105.0	-105.8	,	-106.6	-109.2	,	-100.3	106.3	3 5	-112.3	-106.5	-111.0		-107.4	-111.9		-107.6	-112.1		-109.1	-109.1		-109.0	-108.7	-1094	1130	13.0	-110.1	-109.1	-112.7		-110.5	-109.1		-	-112.1	13.1	11/11
Signal	Leve	"D"	dВ	58.3 -	-79.1	+	-	- 69.7	+	-/3.0	0 32	+	- /4.0	- 76.7	-68.8		-79.1 -1	-71.2 -1						\dashv	+	+	-08.6	╫	+	+-	-+	+	+	╁	┝	-			+	+	+
				-	++	+	-		+	+	+	+	+	-	-			-		-79.7	-71.7			-75.7	+	+	+	-78.1	+	+	-70.0	-77.3	\vdash	-	-80.8	-69.4			-74.0	67.0	+-1
Receive	Antenna Gain	"Ω"	ф	-3.9	-1.0	:	9.	-3.6	- (0.7-	70	710	0.0	-2.6	-7.1		-2.6	-7.1		-2.6	-7.1		-5.0	-5.0		ن د ز	-3.6	-5.0	20	9.0	-7.8	-5.0	-8.6		-5.0	-3.6		-13.3	-8.6	16.0	-10.0
Re	Anter	"Q"	ЯP	20.0	20.0		20.0	31.4	0	7.07	000	2.5	4.17	20.0	27.9		20.0	27.9		20.0	28.0		20.0	21.4		70.07	31.4	20.0	2	4.12	20.0	20.0	21.4		20.0	31.4		20.0	21.4	000	70.07
SSO	pace	"U"	ФВ	132.1	135.7		136.5	136.5	7766	0.4.0	1247	131.7	134.	134.9	134.9		135.7	135.7		135.9	135.9		135.0	135.0	0,50	130.0	136.0	1353	126.2	133.3	133.3	135.0	135.0		136.3	136.3		134.4	134.4	133 1	1.75.1
Path Loss	Free Space	"D"	фB	106.3	127.1		1.621	129.1	9 5 5	0.02	124.0	22.0	0.47	124.7	124.7		127.1	127.1		127.7	127.7		125.1	125.1	000	0.021	0.821	126.1	1261	1.07	118.0	125.3	125.3		128.8	128.8		123.4	123.4	106.0	9.00
		"n"	dBW	31.0	31.0	+	+	30.9		+	31.0	+	+-	31.0	31.0			30.9		Н	30.9		{	30.9	+	+	30.9	30.9	╀	-H	31.0	30.9	╀	H		30.8	\vdash	\dashv	30.9	31.0	+
	EIRP			+	++	+	-	+	+	+	\dashv	╁	+	-							\dashv		-	+	+	+	+	+	╁	+	+	╁	-		<u> </u>	_	\vdash	\dashv	\dashv	╀	+-1
 		"Q"	4BW	28.0	28.0	\dashv	\dashv	28.0	900	+	28.0	+	70.0	-	28.0		_	28.0		Н	28.0		-	28.0	+	+	78.0	28.0	+	++	28.0	28.0	-		_	28.0	Н		28.0	000	+I
	t to Tx	"n.	mi.	23.0	34.7		38.0	38.0	700	2	30.6	200	20.00	31.5	31.5		34.7	34.7		35.5	35.5	_	31.9	31.9	19	2.5.5	35.9	33.1	22 1	33.1	26.3	32.1	32.1		37.2	37.2		29.9	29.9	22.0	7
	Dist	"D"	mi.	1.2	12.9		_	16.2	丄	0.0	0	_		9.7	9.7			12.9			13.8	1		10.2			5.4	11.5	1	لــــــــــــــــــــــــــــــــــــــ	4.5	10.5	10.5		15.7	15.7			4.8	-	
	AZ from Tx	"n"	(a)	352.8	355.7		356.2	356.2	200	0.000	2557	77.00	333.7	355.9	355.9		356.8	356.8		357.4	357.4		356.6	356.6	1	35/39	35/.9	357.7	2677	327.7	355.0	357.5	357.5		359.5	359.5		357.9	357.9	252 2	1,1,1
	AZ fr	"D"	(。)	8.0	1.2	:	4. 4.	4.	9 6	25	3.6		0,0	3.7	3.7		4.1	4.1		5.4	5.4		5.6	5.6	ļ	4.0	4.0	7.9	10	67	7.9	8.1	8.1		9.5	9.5		12.2	12.2	711	2.11
				≱	≱	1	≥	≥	1	\$	3		\$	≱	≽		W	×		W	≩		≱	≱	1	≥ :	≱	≱	3	\$	≥	≱	≽		×	W		≱	≱	3	囗
		tude		7	52		45	45	,	à	26	3 6	S	31	31		14	14		53	53	_	10	2		श्	ရှ	37	37	<u>``</u>	32	42	42		37	37		25	25	22	,
		West Longitude		14	13		13	13		2	13	2 5	21	13	13		13	13		12	12		13	13	9	71	71	12	2	71	13	12	12		11	11		12	12	1.2	2
Receive Site	Coordinates	We	٥	80	80		80	80	5	2	6	2 6	2	20	80		80	80		80	80		80	2	2	2 2	2	80	00	2	80	08	80		80	80		20	2	S	3
Se.	ordi			z	08 Z		z	z		2	7	2 2	z	z	08 Z		z	z		Z	z		08 Z	z	1	2 3	z	z		z	z	z	z		N 80	z	П	2 2	z	2	4
8	ပြ		-	10	23		17	17		2	c		2	37	37		23	23		8	∞		0	0		2 8	2				3	01	10		40	40		17	17	,	
		North Latitude	-		16			19		71		71		13	13		16 2	16			17 8			14		7 5		15 2				4				18			12		
		Nort	•	9 9																											9										0
-	-	-	\vdash	78	56	-	56	22	1	9	75	3 2	1	78	56	H	26	26		26	56		28	8	1	१	7	26	36	۱	28	26	56	-	26	7	H	92	ন	75	1
Rec.	Site	Š	_	R 1	R 2	- 1	R3	R 3	,	보 작	0	216	2	R 6	R 6		R 7	R 7		R 8	ж 8	-	R 9	R 9	9	2 5	R IO	R 11		N 1	R 12	R 13	R 13		R 14	R 14		R 15	R 15	D 16	<u>입</u>

Rec.			Receive Site Coordinates										Path	Loss	Red	ceive	Si	gnal	Total			
Site				Coord						om Tx_		to Tx		RP		Space		na Gain		evel	D/U	
No.	N	North Lat	itude.		V	Vest Lon	gitude		"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	Ratio	
	٥	'	11		0	,	Ħ		(°)	(°)	mi.	mi.	dBW	dBW	dB	dB	dB	dB	dB	dB	dB	
R 17	26	17	44		80	11	1	W	12.5	0.5	14.8	36.2	28.0	30.7	128.3	136.1	20.0	-7.8	-80.3	-113.1	32.8	*
R 17	26	17	44	N	80	11	1	W	12.5	0.5	14.8	36.2	28.0	30.7	128.3	136.1	28.0	-8.0	-72.3	-113.4	41.1	*
														<u> </u>								
R 18	26	14	34	N	80	11	33	W	13.9	359.6	11.1	32.5	28.0	30.8	125.8	135.1	20.0	-13.3	-77.8	-117.6	39.8	*
																			_			
R 19	26	8	56	N	80	13	1	W	14.9	356.2	4.5	26.1	28.0	30.9	118.0	133.2	20.0	-16.0	-70.0	-118.3	48.4	
R 20	26	14	47	N	80	11	1	W	16.2	0.6	11.5	32.8	28.0	30.7	126.1	135.2	20.0	-16.0	-78.1	-120.5	42.4	*
	ļ							1								ļ			ļ <u></u>			$\perp \perp$
R 21	26 26	9	33 33		80	12	42	W	16.3	357.0	5.3	26.8	28.0	30.9	119.3	133.5	20.0	-16.0	-71.3	-118.5	47.2	
R 21	26	9	33	<u> </u>	80	12	42	W	16.3	357.0	5.3	26.8	28.0	30.9	119.3	133.5	21.8	-8.6	-69.5	-111.1	41.6	*
D 00	126		 	1,		<u> </u>	122	1,77	107 1	1 2 1	167	27.7	20.0	20.7	100.0	1264		 		1100	25.	
R 22	26 26	19	1		80 80	9	23	W	17.1	3.1	16.7	37.7	28.0	30.5	129.3	136.4	20.0	-13.3	-81.3	-119.2	37.9	*
R 22	20	19	 	- N	180	19	23	- W	17.1	3.1	16.7	37.7	28.0	30.5	129.3	136.4	28.0	-10.0	-73.3	-116.0	42.6	+
R 23	26	14	13	N	80	11	- -	w	17.2	0.6	10.9	32.1	28.0	30.7	125.6	135.0	20.0	-16.0	77.6	120.2	42.7	+
R 23	26	14	13		80	11	1 1	w	17.2	0.6	10.9	32.1	28.0	30.7	125.6	135.0	21.8	-8.6	-77.6 -75.8	-120.3 -112.9	37.1	+
10 23	20	17	 	+**	-	 	- •	+"	17.2	1.0.0	10.5	32.1	20.0	30.7	123.0	133.0	21.0	-0.0	-/3.6	-112.9	37.1	+-1
R 24	26	8	36	N	80	12	53	w	18.0	356.4	4.2	25.7	28.0	30.9	117.3	133.1	20.0	-16.0	-69.3	-118.2	48.9	+
R 24	26	8	36		80	12	53	w	18.0	356.4	4.2	25.7	28.0	30.9	117.3	133.1	21.8	-8.6	-67.5	-110.8	43.3	+
	+=-	 	1	+		 -	155	╅		1 3 3 3					1	155,1	21.0	0.0	-07.5	-110.0	75.5	+
R 25	26	14	31	N	80	9	43	w	23.0	2.9	11.7	32.5	28.0	30.5	126.3	135.1	20.0	-16.0	-78.3	-120.6	42.3	*
R 25	26	14	31		80	9	43	W	23.0	2.9	11.7	32.5	28.0	30.5	126.3	135.1	21.8	-8.6	-76.5	-113.2	36.7	*
	1			1		_		1-1										0.0	70.5	113.2	30.7	H
R 26	26	14	33	N	80	9	40	w	23.1	3.0	11.7	32.5	28.0	30.5	126.3	135.1	20.0	-16.0	-78.3	-120.7	42.4	*
R 26	26	14	33	N	80	9	40	W	23.1	3.0	11.7	32.5	28.0	30.5	126.3	135.1	28.0	-10.0	-70.3	-114.7	44.4	*
				_																		+
R 27	26	15	11	N	80	9	10	W	24.0	3.9	12.6	33.3	28.0	30.5	126.9	135.3	20.0	-16.0	-78.9	-120.9	42.0	*
																·						
R 28	26	14	25		80	9	25	W	24.6	3.5	11.7	32.4	28.0	30.5	126.3	135.1	20.0	-16.0	-78.3	-120.6	42.4	*
R 28	26	14	25	N	80	9	25	W	24.6	3.5	11.7	32.4	28.0	30.5	126.3	135.1	28.0	-8.6	-70.3	-113.2	43.0	*
- <u>n 00</u>	26	1.5	10	+	-			1		 	165				100						 	
R 29	26	17	45		80	7	5	W	26.7	6.9	16.2	36.4	28.0	30.2	129.1	136.1	20.0	-16.0	-81.1	-121.9	40.9	*
R 29	26	17	45	<u> </u>	80	7	5	W	26.7	6.9	16.2	36.4	28.0	30.2	129.1	136.1	31.4	-3.6	-69.7	-109.5	39.9	*
R 30	26	10	26	NI NI	90	1,		w	26.7	105	7.0	27.0	20 0	20.7	101.0	133.0		160				
N 30	20	10	36	IA	80	11	5	- W	26.7	0.5	7.0	27.9	28.0	30.7	121.8	133.8	20.0	-16.0	-73.8	-119.1	45.3	\square
R 31	26	10	27	N	80	11	8	w	27.0	0.4	6.8	27.8	28.0	30.7	121.6	133.8	20.0	160	72.6	1101	15.5	
R 31	26	10	27		80	11	8	w	27.0	0.4	6.8	27.8	28.0	30.7	121.6	133.8	20.0	-16.0	-73.6 -65.6	-119.1 -116.6	45.5	\vdash
11/31	120	1.0	- 121		00	11		-	27.0	U.T	U.8	21.0	20.0	30.7	121.0	133.0	20.0	-13.5	-0.2.0	-110.0	51.0	\vdash
R 32	26	16	44	N	80	7	27	w	27.4	6.5	15.0	35.2	28.0	30.2	128.4	135.8	20.0	-16.0	-80.4	-121.7	41.2	*
R 32	26	16	44		80	7	27	w	27.4	6.5	15.0	35.2	28.0	30.2	128.4	135.8	31.4	-3.6	-69.0	-109.3	40.2	*
11,52	120	 ``		+**		- '		+"	<u> </u>	 " 	13.0	33.2	20.0	30.2	120.7	133.0	71.7	-5.0	-07.0	-107.3	40.4	
<u> </u>					1																	

Rec.	1			Recei	ve Site											Loss		ceive		gnal	Total	I
Site				Coord	linates				AZ fro			to Tx		RP		Space		na Gain		evel	D/U	
No.	N	lorth Lati	tude.			est Long			"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	Ratio	
	0		"	\mathbb{I}_{-}	۰	'	- 11		(°)	(°)	mi.	mi.	dBW	dBW	dB	dB	dB	dB	dB	dB	dB	\perp
R 33	26	18	31		80	6	24	W	27.5	7.8	17.3	37.4	28.0	30.1	129.7	136.4	20.0	-16.0	-81.7	-122.3	40.6	*
R 33	26	18	31	N	80	6	24	W	27.5	7.8	17.3	37.4	28.0	30.1	129.7	136.4	27.9	-7.1	-73.8	-113.4	39.6	*
 	1			 				1		2240						1000	20.0					4-4
R 34	26	6	32		80	13	20	W	27.5	354.9	1.8	23.4	28.0	31.0	110.0	132.3	20.0	-16.0	-62.0	-117.3	55.3	-
R 34	26	6	32	N	80	13	20	W	27.5	354.9	1.8	23.4	28.0	31.0	110.0	132.3	28.0	-14.0	-54.0	-115.3	61.3	
D 26	- 06	 	-	1	00	7	26	- 337	27.0	6.6	140	35.0	28.0	30.2	1202	1260	20.0	160	90.2	121.6	41.2	*
R 35	26	16	33	+N	80		20	W	27.8	0.0	14.8	33.0	28.0	30.2	128.3	135.8	20.0	-16.0	-80.3	-121.6	41.3	+
R 36	26	10	26	NI	80	11	2	w	27.8	0.6	6.9	27.8	28.0	30.7	121.6	133.8	20.0	-16.0	-73.6	-119.1	45.4	+
130	20	10	20	IN	80	11		 '' 	27.0	0.0	0.9	27.0	20.0	30.7	121.0	133.8	20.0	-10.0	-/3.0	-117.1	73.7	+
R 37	26	19	10	N	80	5	44	w	28.3	8.7	18.3	38.2	28.0	30.0	130.1	136.6	20.0	-16.0	-82.1	-122.6	40.4	*
- X 3 /	-	1	1.0	+**		 	- 	+ "		1								1		122.0		1
R 38	26	17	44	N	80	6	31	W	28.5	7.8	16.5	36.5	28.0	30.1	129.2	136.1	20.0	-16.0	-81.2	-122.1	40.8	*
				1			1															
R 39	26	14	41	N	80	8	16	W	28.9	5.5	12.5	32.8	28.0	30.3	126.8	135.2	20.0	-16.0	-78.8	-120.9	42.1	*
													-									
R 40	26	18	29		80	5	52	W	29.1	8.7	17.5	37.5	28.0	30.0	129.8	136.4	20.0	-16.0	-81.8	-122.4	40.6	*
R 40	26	18	29	N	80	5	52	W	29.1	8.7	17.5	37.5	28.0	30.0	129.8	136.4	31.4	-3.6	-70.4	-110.0	39.6	*
B 41			-	+	00		7	-	20.4	1 72	140	346	20.0	30.1	100.0	106.7	00.0	160	00.2	101.7	41.4	+
R 41	26 26	16	21		80 80	7	7	W	29.4 29.4	7.2	14.8	34.8 34.8	28.0 28.0	30.1 30.1	128.3 128.3	135.7 135.7	20.0	-16.0 -11.0	-80.3 -72.3	-121.7 -116.7	41.4	-
K 41	20	10	21	14	180		- '	W	29.4	1.4	14.0	34.0	28.0	30.1	128.3	133.7	28.0	-11.0	-/2.3	-110.7	44.4	+
R 42	26	15	46	N	80	7	27	w	29.5	6.8	14.0	34.1	28.0	30.2	127.8	135.6	20.0	-16.0	-79.8	-121.4	41.6	*
R 42	26	15	46		80	7	27	w	29.5	6.8	14.0	34.1	28.0	30.2	127.8	135.6	21.4	-12.4	-78.4	-117.8	39.4	+
 		1	1	+:-		- ′		+**+	27.0	9.0		J 112	20.0	50.2	127.0	133.0	21.3	12.7	70.7	117.0	37.4	
R 43	26	14	52	N	80	8	0	W	29.6	6.0	12.8	33.0	28.0	30.3	127.1	135.3	20.0	-16.0	-79.1	-121.0	41.9	*
R 43	26	14	52		80	8	0	w	29.6	6.0	12.8	33.0	28.0	30.3	127.1	135.3	31.4	-3.6	-67.7	-108.6	40.9	*
R 44	26	14	27	N	80	8	3	W	30.5	6.0	12.4	32.6	28.0	30.3	126.8	135.2	20.0	-16.0	-78.8	-120.9	42.1	*
R 44	26	14	27	N	80	8	3	W	30.5	6.0	12.4	32.6	28.0	30.3	126.8	135.2	28.0	-13.0	-70.8	-117.9	47.1	
<u> </u>	-						<u> </u>	1.1														
R 45	26	7	25		80	12	39	W	30.5	356.8	3.0	24.3	28.0	30.9	114.5	132.6	20.0	-16.0	-66.5	-117.7	51.2	
R 45	26	7	25	N	80	12	39	W	30.5	356.8	3.0	24.3	28.0	30.9	114.5	132.6	21.4	-10.3	-65.1	-112.0	46.9	
D 46	26	14	- 60	1	90		20	137	21.4		12.2	22.2	20.0	20.0	107.2	1272	20.0	160	70.3	121 1	41.0	+
R 46	26	14	59	12	80	_ 7	28	W	31.4	6.9	13.2	33.2	28.0	30.2	127.3	135.3	20.0	-16.0	-79.3	-121.1	41.8	\dashv
R 47	26	15	45	N	80	6	49	w	31.8	7.8	14.3	34.2	28.0	30.1	128.0	135.6	20.0	-16.0	-80.0	-121.5	41.5	\dashv
R 47	26	15	45		80	6	49	w	31.8	7.8	14.3	34.2	28.0	30.1	128.0	135.6	28.0	-13.2	-72.0	-118.7	46.7	$\overline{}$
 		1.5	 	1,4	-	 	+	+"+	J 1.0	1.0		J 7.60	20.0	30.1	120.0	133.0	20.0	-13.2	-, 2.0	140.7	10.7	
R 48	26	16	48	N	80	6	4	w	31.9	8.8	15.8	35.5	28.0	30.0	128.9	135.9	20.0	-16.0	-80.9	-121.9	41.1	1
R 48	26	16	48		80	6	4	W	31.9	8.8	15.8	35.5	28.0	30.0	128.9	135.9	28.0	-13.2	-72.9	-119.1	46.3	
				1																		\Box
R 49	26	14	9	N	80	7	13	W	34.6	7.6	12.6	32.3	28.0	30.1	126.9	135.1	20.0	-16.0	-78.9	-121.0	42.1	*

Rec.	T			Recei	ve Site		_,,				_					Loss	Re	ceive	Si	gnal	Total	
Site				Coord	linates				AZ fro			to Tx		RP		Space		na Gain		evel	D/U	
No.	N	orth La	titude.		V	est Lon	gitude		"D"	"U"	"D"	"U"	"D"	"U"	"D"_	"U"	"D"	"U"	"D"	"U"	Ratio	
	٥	,	"		•	'	"		(°)	(°)	mi.	mi.	dBW	dBW	dB	dB 1	dB	dB	dB	dB	dB	
R 49	26	14	9	N	80	7	13	W	34.6	7.6	12.6	32.3	28.0	30.1	126.9	135.1	21.4	-9.9	-77.5	-114.9	37.4	*
					<u></u>																	
R 50	26	13	9		80	7	45	W	35.6	6.8	11.3	31.1	28.0	30.2	126.0	134.8	20.0	-16.0	-78.0	-120.6	42.6	*
R 50	26	13	9	N	80	7	45	W	35.6	6.8	11.3	31.1	28.0	30.2	126.0	134.8	31.4	-3.6	-66.6	-108.2	41.6	*
					.					1												44
R 51	26	8	22		80	11	33	W	35.8	359.5	4.6	25.4	28.0	30.8	118.1	133.0	20.0	-16.0	-70.1	-118.2	48.1	
R 51	26	8	22	N	80	11	33	W	35.8	359.5	4.6	25.4	28.0	30.8	118.1	133.0	31.4	-5.6	-58.7	-107.8	49.1	1
7 50		1		1	00	-	22	-	36.7	0.0	13.1	32.6	200	20.0	127.3	135.2	20.0	160	70.2	101.0	41.0	*
R 52	26 26	14	18 18		80 80	6	32 32	W	36.7	8.8	13.1	32.6	28.0 28.0	30.0 30.0	127.3	135.2	20.0 31.4	-16.0 -14.0	-79.3 -67.9	-121.2 -119.2	41.9 51.3	+
K 32	26	- 14	18	- N	80	<u> </u>	32	+*	30.7	0.0	13.1	32.0	20.0	30.0	127.3	133.2	31.4	-14.0	-67.9	-119.2	31.3	+
R 53	26	14	11	N	80	6	38	w	36.7	8.6	12.9	32.4	28.0	30.0	127.1	135.1	20.0	-16.0	-79.1	-121.1	42.0	*
R 53	26	14	11		80	6	38	w	36.7	8.6	12.9	32.4	28.0	30.0	127.1	135.1	21.4	-9.9	-77.7	-115.0	37.3	*
1033	20	1.	- • • • • • • • • • • • • • • • • • • 	+*`	100	 	-	+"	30.7	1 0.0			20.0	30.0		155.1		7.5	ļ <i>'.'</i>	113.0		+
R 54	26	11	47	N	80	8	34	w	37.0	5.6	9.5	29.4	28.0	30.3	124.5	134.3	20.0	-16.0	-76.5	-120.0	43.5	*
R 54	26	11	47		80	8	34	w	37.0	5.6	9.5	29.4	28.0	30.3	124.5	134.3	21.4	-10.3	-75.1	-114.3	39.2	*
			_																			\Box
R 55	26	9	31	N	80	10	26	W	37.3	2.0	6.3	26.7	28.0	30.6	120.9	133.4	20.0	-16.0	-72.9	-118.8	45.9	
R 56	26	8	22		80	11	23	W	37.5	359.9	4.7	25.4	28.0	30.8	118.3	133.0	20.0	-16.0	-70.3	-118.2	47.9	
R 56	26	8	22	N	80	11	23	W	37.5	359.9	4.7	25.4	28.0	30.8	118.3	133.0	28.0	-14.0	-62.3	-116.2	53.9	
	- 	 	_	 	ļ	_	 			1					ļ							
R 57	26	9	21		80	10	32	W	37.6	1.8	6.1	26.5	28.0	30.6	120.6	133.4	20.0	-16.0	-72.6	-118.7	46.1	
R 57	26	9	21	- N	80	10	32	W	37.6	1.8	6.1	26.5	28.0	30.6	120.6	133.4	31.4	-10.6	-61.2	-113.3	52.1	
R 58	26	12	5	NI.	80	8	1	w	38.4	6.6	10.2	29.8	28.0	30.2	125.0	134.4	20.0	-16.0	-77.0	-120.2	43.2	-
R 58	26	12	5		80	8	1	w	38.4	6.6	10.2	29.8	28.0	30.2	125.0	134.4	31.4	-9.1	-65.6	-113.3	47.7	
1130	- 20		- 	- ``	00	- -	 • • • • • • • • • • • • • • • • • • •	- '' 	30.4	1 0.0	10.2	27.0	20.0	30.2	125.0	157.7	31.4	-7.1	-03.0	-113.3	7/./	
R 59	26	11	41	$\frac{1}{N}$	80	8	17	W	38.8	6.2	9.6	29.4	28.0	30.2	124.6	134.3	20.0	-16.0	-76.6	-120.1	43.5	*
R 59	26	11	41		80	8	17	w	38.8	6.2	9.6	29.4	28.0	30.2	124.6	134.3	28.0	-14.0	-68.6	-118.1	49.5	П
		1		<u> </u>																		
R 60	26	6	10		80	13	13	W	39.0	355.1	1.5	22.9	28.0	31.0	108.4	132.1	20.0	-16.0	-60.4	-117.2	56.7	
R 60	26	6	10	N	80	13	13	W	39.0	355.1	1.5	22.9	28.0	31.0	108.4	132.1	21.4	-12.6	-59.0	-113.8	54.7	
R 61	26	10	35	N	80	9	9	W	39.5	4.6	8.1	28.0	28.0	30.4	123.1	133.8	20.0	-16.0	-75.1	-119.5	44.4	*
<u> </u>					ļ			4														
R 62	26	7	37		80	11	43	W	41.4	359.1	3.8	24.5	28.0	30.8	116.4	132.7	20.0	-16.0	-68.4	-117.9	49.5	
R 62	26	7	37	<u>N</u>	80	11	43	W	41.4	359.1	3.8	24.5	28.0	30.8	116.4	132.7	28.0	-14.0	-60.4	-115.9	55.5	\dashv
D 62		10		+			121	117	41.7	- 0.3	110	20.0	20.0	20.0	104.4	1245	- 20.0	160	70.4	1000	10.5	_
R 63	26 26	12	50		80	6	31	W	41.7	9.3	11.8	30.9	28.0	29.9	126.4	134.7	20.0	-16.0	-78.4 70.4	-120.8	42.5	-
K 03	20	12	120	1N	80	 0	31	- W	41.7	9.3	11.8	30.9	28.0	29.9	126.4	134.7	28.0	-14.0	-70.4	-118.8	48.5	-
R 64	26	11	31	NI	80	7	46	w	42.0	7.2	9.8	29.2	28.0	30.1	124.8	134.2	20.0	-16.0	-76.8	-120.1	43.4	*
17/04	140	111	121	14	Too.	/	טדן	1 77	74.0	<u> ۱۰۴</u>	2.0	47.6	20.0	20.1	144.0	134.2	20.0	-10.0	-/0.0	-12V.I	7.7.7	

1	ato T	gusl	!S	eive:	Яес	ross	Path							<u> </u>			e Site					,09 <i>5</i>	
	<u>n/c</u>	ləvə	r	na Gain		Space		<u>"тт"</u>		XT of:			hà SA "G"	╁╼╌┞	abirti,	1 +36	inates),00rd		1 Amo	14	Site	
	Ratio	"n.	"D"	"U"	"D"	μΩ _#	"D"	"Ω"	"D"	"U"	"D"	"U"	"D"	-	יוחמב:	est Long	M		נחמכי	orth Lati	o Ni	.oV	<u></u>
+	BP	ЯP	ЯР	ЯÞ	ЯР	Вb	ЯР	PBW	PBW	.im	·ıw	(.)	(,)	\vdash									-
- -	2.74	£.811-	1.17-	0.81-	0.02	133.0	1.911	30.6	0.82	25.3	1.2	8.1	<i>L.</i> ≥₽	W	34	01	08	N	11	8	97	\$ 9	Я
	2.52	£.611-	1.53-	0.41-	0.82	133.0	1.911	3.0£	0.82	25.3	1.2	8.1	L'SÞ	M	34	01	08		L1	8	97		В
														111			00	-``		0			۳
	0.74	2.811-	4.17-	0.31-	0.02	133.0	4.911	2.05	0.82	25.4	£.2	1.2	7.24	M	LC	10	08	N N	73	8	76 76	99	R R
	0.52	2.911-	4.59-	0.41-	0.82	0.551	4 .911	30.5	0.82	25.4	€.2	1.2	7.24	M	LZ	01	Λο	NI I	C7	0	07	00	<u></u>
- -	8.84	0.811-	2.69-	0.91-	0.02	132.7	117.2	7.05	0.82	24.6	1.4	2.0	T.24	M	91	11	08	N	01		56	<u></u>	Я
	8.48	0.611-	2.13-	0.01-	0.82	132.7	2.711	7.05	0.82	24.6	l'Þ	2.0	T.24	M	91	II	08		0t	L	97		Я
		2125																					=
*	1,44	č .611-	4.27-	0.31-	0.02	T.EEI	123.4	30.2	0.82	2.72	₽. 8	6.9	7.74	M	L	8	08	N	b	01	97	89	Я
+				0).	0 00	7 001	7 (()	202	0.80	LYC	> L	09	1 07	1/10	38	8	08	N	97	6	56	65	Я
*	8.44	2.911-	p.p/-	0.81-	0.02	133.4	122.4	€.0€	0.82	7.92	¿.r	0.9	1.64	M	- 00		00	L.	07		^-		<u> </u>
	1.94	9.811-	2.2T-	0.91-	0.02	1.551	120.5	2.0£	0.82	23.6	0.9	8.5	2.64	M	77	6	08	N	33	. 8	97	0/	Я
	1.0+	0.611-	C'71-	0.01	0:07	1.001	610.51	510.7	4155														
	8.24	7.811-	6. 2 7-	0.81-	0.02	1.551	120.9	≱. 0£	0.82	25.6	€.3	6.4	0.52	M	ÞI	6	08		82	8	97	14	Я
	8.12	7.311-	6.43-	0.41-	0.82	1.551	120.9	30.4	0.82	9.22	£.8	6.4	0.52	M	14	6	08	N	82	8	97	1/	В
							0 00.	, 00	7 80	0.30	0 >	'	دن ه	\mathred{u}	76	0	08	IN.	8	8	90	CL	q
	4.84	2.811-	2.27-	0.81-	0.02	132.9	2.021	4.0£	28.0	25.2	8.č	['t	8.£2 8.£2	M	9E 9E	6		N N	8	8	7 <u>9</u> 79	7/	В В
	4.22	5.311-	2.43-	0.41-	0.82	6.251	2.021	4.00	0:07	7:07	0.0	ļ	0100	1									
*	6.44	1.911-	2.47-	0.91-	0.02	2.551	122.2	2.08	0.82	1.92	£.7	7.9	5.42	M	23	8	08	N	53	8	97		В.
	6.02	7.511-	8.29-	9.01-	31.4	2.EEI	122.2	30.2	0.82	1.62	€.7	<i>L</i> .8	54.2	M	23	8		N	23	8	56	£1	8
									† - • • •		· •	0 270	- /3	111	• • •	- 01		1.4	01		70	VI	† a
	7.22	£.711-	2.49-	0.51-	0.02	1.251	2.211	30.9	0.82	0.52	2.4	8.72£	7.88	M	II II	15 15		N N	18	9	79 79	7/	В
-	2.52	4.811-	1.69-	1.21-	4.12	1.251	2.211	6,0€	0.82	0.52	2.4	0.100	/'00	-		71		,	- 4		~=		
*	44.2	2,911-	0.2 <i>T</i> -	0.91-	0.02	133.2	123.0	0.0£	0.82	0.92	0.8	6.8	7.62	W	97	۷	08	N	40	8	97	Ş	В.
	2.02	8.611-	9.£9-	9.01-	4.15	133.2	123.0	30.0	0.82	0.62	0.8	6.8	L'6\$	M	97			N	40	8	97	SI	В
							1	<u> </u>	1	","	- <u>`</u>		- 07	111	20		V 8	1.4	76	- 6	96	71	 a
*	44.3	6.611-	0.27-	0.51-	0.02	133.2	123.0	6.62	0.82	0.92	0.8	1.6	4.09	M	73 73			N	9E	8	76 78	9/	ਬ
\vdash	5.05	6.511-	9.£9-	9.01-	31.4	2.551	123.0	6.62	0.82	0.92	0.0	110	F.VV	 	-								Ļ
	6.94	1.811-	2.17-	0.91-	0.02	132.6	2.911	2.0£	0.82	24.3	2.2	3.9	۲٬09	W	77	6	08	N	77	L	97	L	Ŋ
	6.28	1.611-	2.£9-	0.41-	0.82	132.6	119.2	₹.0€	0.82	24.3	2.2	3.9	7.09	M	77	6	08	N	77	L	97	L	В.
													0.05	 	``			1				01	۲
	46.3	E.811-	0.27-	0.91-	0.02	7.281	120.0	30.4	0.82	24.5	7.8	6.4	0.13	W	61	6		N	33	L	92		Ы
	\$2.3	£.311-	0.49-	0.41-	0.82	7.281	0.021	\$0.4	0.82	24.5	T.č	6.4	0.13	M	61	6	00	N	33	L	97	0.	Я
	2 07	LLII	1 89	091-	1 0 02	132.3	116.4	30.6	0.82	23.4	8.£	1.1	62.3	M	22	10	08	N	40	9	97	6/	В.
H	£.02	F.711-	4.89-	0.81-	20.02	132.3	1.011	3.05	0.82	23.4	8.8	1,1	62.3	M	\$\$	10		N	40	9	97		В
	C:0C	CLITY	0:10	O'CT	117.07	00-	44077																4

				*	T	Ī					\top		T	T		_			_					1	T	1			П		·	T		11	Т	_			
Total	DYC	Ratio	₽ B	44.0	46.9	52.9	55.5		47.6	46.6	7.07	48.0	24.0	52.1		45.1	51.1		45.5	51.5		45.7		45.8		51.4	54.8	45.1		45.9	51.9		c.0c	46.2	0,77	40.8	52.8	72.8	47.3
Signal	Level	<u>"</u> 0	왕	-119.2	-1181	-112.7	-117.0		-117.9	-109.0	,	0'/11-	-115.6	-117.2		-118.7	-116.7		-118.3	-116.3		-118.2		-118.2		-117.1	-119.1	-118.2		-117.8	-115.8		-117.0	-117.6		-11/.2	-111.9	-119.6	-119.2
Sig	Le	"Ω"	ф	-75.2	-71.2	-59.8	-61.5		-70.3	-62.4		0.60-	0.10	-65.1		-73.6	-65.6		-72.8	-64.8		-72.6		-72.4		-63.7	-64.3	-73.0		-71.9	-63.9		-00.0	-71.3	-+	+	-59.1	-46.9	-71.9
Receive	Antenna Gain	"Ω"	æ	-16.0	-16.0	-10.6	-16.0		-16.0	-7.1	0,51	0.01-	-14.0	-16.0		-16.0	-14.0		-16.0	-14.0		-16.0		-16.0		-16.0	-18.0	-16.0		-16.0	-14.0	3	0.0	-16.0	99	-10.0	-10.6	-19.0	-18.6
Rec	Antenn	"D"	æ	20.0	20.0	31.4	20.0		20.0	27.9	000	0.02	7.07	20.0		20.0	28.0		20.0	28.0		20.0		20.0	100	70.0	21.4	20.0		20.0	28.0	6	0.02	20.0	6	20.07	31.4	20.0	20.0
Loss	pace	"n"	æ	133.1	132.5	132.5	131.9		132.3	132.3	132.2	7.761	136.2	132.0		132.7	132.7		132.4	132.4		132.4		132.4		131.8	131.8	132.2		132.0	132.0	7	7.16	131.8	1216	0.101	131.6	131.6	130.8
Path Loss	Free Space	"D"	ф	123.2	119.2	119.2	109.5		118.3	118.3	117.0	01/10	0./11	113.1		121.6	121.6		120.8	120.8		120.6		120.4	2 4 4 4 4	113./	113.7	121.0		119.9	119.9	1116	114:3	119.3	110 6	110.3	118.5	94.9	119.9
	ያ	"n"	dBW	29.9	30.4	30.4	30.9		30.5	30.5	30.5	20.00	30.0	30.8		30.0	30.0		30.1	30.1		30.2		30.2	9 00	50.5	30.8	30.0		30.2	30.2	100	30.	30.2	20.3	20.3	30.3	31.0	30.2
	EIRP	"D"	dBW	28.0	28.0	28.0	28.0		28.0	28.0	0 80	20.00	7.07	28.0		28.0	28.0		28.0	28.0		28.0		28.0	6	0.62	28.0	28.0		28.0	28.0	000	70.0	28.0	28.0	2:0:	28.0	28.0	28.0
	Dist to Tx	"U"	mi.	25.8	23.9	23.9	22.4		23.5	23.5	22.7	4.55	7:67	22.7		24.4	24.4		23.8	23.8		23.7		23.6	5	7.77	22.2	23.0	,	22.6	22.6	22.0	77.0	22.1	216	2	21.6	21.7	19.7
	Dist	"D"	mi.	8.2	5.2	5.2	1.7		4.7	4.7	4.0	2 2	2	2.6		8.9	8.9		6.2	6.2		6.1	,	5.9	9	0.7	2.8	6.4	,	2.6	2.6	30	3	5.3	8 4	2	4. ∞	0.3	5.6
	from Tx	"C	(6)	8.6	4.4	4.4	356.6		3.4	3.4	2.0	2 6	7:0	358.6		8.2	8.2		7.3	7.3		7.0	,	8:0	360 6	2.77.3	359.5	8.5	,	8.9	8.9	0 3	3	6.2	4.0	,,,	2.0	353.2	8.9
	AZ fi	"D"	(၁)		65.4	\sqcup	0.99		66.5		1 66.7	\perp	↓_	7.99			68.3	\perp	71.7	\perp	_	72.0		72.4				79.7	\perp	81.4		63 1	<u> </u>	86.9	\bot			100.5	111.6
				≱		≯	 ≱	-	≱	*		=		≱	+	W	*		≱		\dashv	≱	+	≯	=	≱ :	≯	≱	-	≱	}	3		≱	3		≱	≱	≱
		West Longitude		4	35	35	38	_	29	29	22	3 6	3	51		29	89		24	77		33	_	25	33	7 5	32	7		5	2	13	2	7	20	3 3	30	20	4
		st Lor	-	7	6	6	12	_	0	6	2	2 5	2	=		7	-		∞	∞		∞		×	=	: :	= _	∞		×	••	=	-	6	0		6	13	6
Receive Site	Coordinates	We	0	% Z	2	08 Z	08 N		08 Z	&	Ca	3 8	8	08 Z		8 Z	80		08 Z	80		& Z		2	Va	00 5	2	08	8	20	<u></u>	2	3	80	80	3 3	08	08 Z	N 80
Recei	Coord			Z	Z	Z	z	_	z	z	2	2		z		Z	z	-	Z	Z	<u> </u>	Z	<u> </u> ;	Z	7	- 7	Z	z	-	z į	Z.	2	-	z	Z		Z	z	z
		titude.	Ξ.	56	-		45		9	46	3.2	3 5	75	2		77	21		21	-51		47		5	4	2 9	5	6	-	2	53	28	3	24	2		7	9	21
		North Latitude.	-	••	7	7	8	-	9	9	Y) v	}	9	•	_	7		9	9		9		٥	v		_	ع	-	_	<u>c</u>	6	<u> </u>	S	\ <u>\</u>	,	^	8	3
_	_		°	56	79	97	26		92	92	76	2,42	3	56		56	92		56	28	,	22	1	9	7	3 2	97	56	1	9	8	26	1	56	36		97	56	56
Rec.	Site	No.		R 80	R 81	R 81	R 82	- ;	R 83	R 83	R 84	780	5	R 85		R 86	R 86		R 87	R 87		R 88	000	K 09	00	2 2	N N	R 91	5	K 22	K 72	R 03	2	R 94	R 95	200	2 2	R 96	R 97

						7	Τ					T	1	Γ					\top		_		\top	Τ		Т	$\overline{}$	<u> </u>	7	11	_	*	1		1 1	
Total	⋛	Ratio	₽P	50.7	46.5	45.0	48.7		47.9		47.6	47.8	46.4	48.3		45.7	46.5	7 8 6	2001	55.1	53.4	0 03	6.00	47.1	46.3	47.1	46.1	7 7 7 7	53.4	1.00	45.4	41.2	46.9	45.6	47.0	46.0
Signal	vel	"U"	фB	-114.6	-119.4	1106	-114.3		-120.1		-120.0	-118.8	-120.1	-110.6		-120.6	-110.0	1213	0111	-123.2	-113.6	3 001	C.771-	-121.5	-109.3	121.6	-109.2	2000	112 5	2011	-121.1	-108.9	-121.7	-109.0	-121.7	-121.6
Sig	Level	"D"	dВ	-63.9	-73.0	-717	-65.7		-72.1		-72.4	-71.0	-73.8	-62.4		-74.9	-63.5	77.8	0:1	-68.1	-60.1	71.6	0.1/-	-74.4	-63.0	-74.5	,	107	+	++	\dashv	-67.7	-74.8	+	-74.7	-75.5
Receive	Antenna Gain	"U"	dВ	-14.0	-18.9	-103	-14.0		-19.8		-19.8	-18.6	-20.1	-10.6		-21.2	-10.6	210	213	-23.6	-14.0	7 22	4.67-	-22.8	-10.6	-23.0	-10.6	27.2	140	2:1	-22.8	-10.6	-23.2	-10.6	-23.4	-23.6
Rec	Antenn	"D"	đВ	28.0	20.0	20.0	28.0		20.0		20.0	21.4	20.0	31.4		20.0	31.4	000	2	20.0	28.0	000	2.03	20.0	31.4	20.0	31.4	000	280	203	20.0	28.0	20.0	31.4	20.0	20.0
Loss	pace	"C"	ФВ	130.8	130.5	130.2	130.2		130.4		130.4	130.4	129.9	129.9		129.2	129.2	1207		130.4	130.4	1001	1.63.7	128.9	128.9	128.8	128.8	120.4	130.4	1	128.3	128.3	128.6	128.6	128.6	128.1
Path Loss	Free Space	ľΩ	фB	119.9	121.0	1217	121.7		120.1		120.4	120.4	121.8	121.8		122.9	122.9	120.8		116.1	116.1	7011	117.0	122.4	122.4	122.5	122.5	1311	1161		123.7	123.7	122.8	122.8	122.7	123.5
	2	<u>.</u>	dBW	30.2	30.0	29.9	29.9		30.2		30.2	30.2	29.9	29.9		29.8	29.8	303		30.8	30.8	30.6	2:27	30.2	30.2	30.2	30.2	30.0	300		30.0	30.0	30.2	30.2	30.3	30.2
	EIRP	μΩ.	dBW	28.0	28.0	28.0	28.0		28.0		28.0	28.0	28.0	28.0		28.0	28.0	28.0		28.0	28.0	0 00	7.0.7	28.0	28.0	28.0	28.0	28.0	280		0.82	28.0	28.0	28.0	28.0	28.0
	Dist to Tx	<u>"</u>	mi.	19.7	19.1	18.5	18.5		18.9		18.7	18.7	17.9	17.9		16.5	16.5	17.4		18.8	18.8	17.4		15.8	15.8	15.7	15.7	18.7	18.7		14.8	14.8	15.3	15.3	15.3	14.4
	Dist	"D	mi.	9.6	6.3	0.9	6.9		5.8		5.9	5.9	7.0	7.0		7.9	7.9	62		3.6	3.6	4.4	;	7.5	7.5	7.6	7.6	3.6	3.6		ò./	8.7	7.9	7.9	7.8	9.8
	AZ from Tx	Ţ.	(၃)	8.9	8.6	9.7	╁		6.4		8.9	8.9	9.2	9.2		10.1	10.1	5.3		358.3	358.3	1.7		6.2	6.2	6.2	6.2	357.8	357.8		×,	8.7	6.3	6.3	5.6	6.4
	AZ fr	ָה ה	(၃)	111.6	115.4	1196	↓		119.8			120.6	124.8				133.2	133.6	1		140.1	140.0	1_		142.2	142.8	\perp	143 3	┶	1-1-	143.9	l_	144.5	144.5	145.6	148.3
				≱		3	≥		≱	_	≥	≱	≱	≯		≽	≱	_ ≥	:	≱	≱	3	-	≥	A	>	≽	3	≥		≱	≱	≥	≱	≥	≱
		gitude	=	4	35	02	19		17	-	=	=	35	35		32	32	46		52	52	Ş	3	41	41	42	42	-	2		2	2	43	43	53	47
		West Longitude	-	6	∞	00			6		6	6	∞	œ		∞	œ	0		Ξ	=	2	2	6	6	6	6	12	12		7	٥	6	6	6	6
Receive Site	Coordinates	_	0	08 N	08 N	2	08 Z		08 N	_		08 Z	08 Z	08 Z		08 Z	08	2		08 Z	08 Z	2		80	08 N	08 Z		0	2 2		2	8 Z		08 Z	0 8	08 Z
Rec	ပိ		H	7	+++	+		\vdash		+		-	_			7	-	-	H		7	+	1			-	\Box	- -	1	+	7	+	_	7	+	+
		ntitude.	=	21	47	=	=		39	_	31	31	41	41		92	56	25		43	43	30	3	0	0	2	24	37	37		7	7	35	35	35	49
	, i	North Latitude.	<u>.</u>	3	2	,	2		2	_	7	2	1		-	0	0		-	7	7	-	-	0	0	59	59	-	2		?	29	59	59	59	58
	-		°	26	56	26	56		26	-	56	56	26	56		56	56	26		56	26	7,	3	26	76	25	25	26	56		3		25	25	25	25
Rec.	Site	No.		R 97	R 98	8	R 99		R 100	_	R 101	R 101	R 102	R 102		R 103	R 103	R 104		R 105	R 105	R 106	3	R 107	R 107	R 108	R 108	R 109	R 109	-	N I I	R 110	R 111	R ====================================	R 112	R 113

	Rec.			1	Recei	ve Site										Path	Loss	Re	ceive	Si	gnal	Total	\perp
	Site				Coord	linates				AZ fro			to Tx		RP		Space		na Gain		evel	D/U	
	No.		orth Lat	itude.		N.	est Lon	gitude		"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	Ratio	
		-		"		°		**		(°)	(°)	mi.	mi.	dBW	dBW	dB	dB	dB	dB	dB	dB	dB	
		 			ļ				 						\				<u> </u>	ļ		.	
R	114	26	1	50	N	80	11_	56	<u> </u>	149.2	358.0	4.4	17.8	28.0	30.8	117.8	129.9	20.0	-25.0	-69.8	-124.1	54.3	ļ
<u> </u>	110	-	 		٠	-	 		117	152.0			160		20.0	101.0	1000				1		
K	115	26	0	13	IN.	80	11	20	W	153.0	0.0	6.4	16.0	28.0	30.7	121.0	129.0	20.0	-25.0	-73.0	-123.3	50.3	
- D	116	26	 	53	1	80	12	29	w	155.6	356.2	4.1	17.9	28.0	30.9	117.2	130.0	20.0	-25.0	-69.2	124.0	54.0	+
H	110	20	1	33	114	ov	12	23		133.0	330.2	7.1	17.9	28.0	30.9	117.2	130.0	20.0	-23.0	-09.2	-124.0	54.8	+-
R	117	25	58	44	TN.	80	11	31	w	159.9	359.2	7.9	14.3	28.0	30.8	122.8	128.0	20.0	-25.0	-74.8	-122.2	47.4	+
	117	25	58	44		80	111	31	W	159.9	359.2	7.9	14.3	28.0	30.8	122.8	128.0	27.9	-8.1	-66.9	-105.3	38.4	*
			+	 	+	-	1	- 	1								120.0		†	30.5	100.0	30	+-
R	118	26	2	24	N	80	13	4	w	160.8	354.5	3.3	18.6	28.0	31.0	115.4	130.3	20.0	-25.0	-67.4	-124.3	56.9	1
	119	25	58	40	_	80	11	51	W	162.4	357.8	7.8	14.2	28.0	30.9	122.8	127.9	20.0	-25.0	-74.8	-122.1	47.3	
R	119	25	58	40	N	80	11	51	W	162.4	357.8	7.8	14.2	28.0	30.9	122.8	127.9	27.9	-8.1	-66.9	-105.2	38.3	*
_	100	1		4.	٠	-	-		 	166.7	254.5		16.6	22.2									
K	120	26	0	41	N	80	12	52	W	165.7	354.5	5.3	16.6	28.0	31.0	119.4	129.3	20.0	-25.0	-71.4	-123.3	51.9	4-4
R	121	26	0	38	N	80	13	4	w	168.0	353.8	5.3	16.5	28.0	31.0	119.4	129.3	20.0	-25.0	-71.4	-123.3	51.9	-
	121	26	0	38		80	13	4	w	168.0	353.8	5.3	16.5	28.0	31.0	119.4	129.3	31.4	-12.6	-60.0	-110.9	50.9	+
- 1		1	 	1	† 		1								71.0	*****	127,5	J1.1	12.0	-00.0	110.5	20.7	+-1
R	122	25 25	56	41	N	80	12	16	W	168.8	355.4	9.9	11.9	28.0	31.0	124.8	126.4	20.0	-25.0	-76.8	-120.5	43.7	*
R	122	25	56	41	N	80	12	16	Ŵ	168.8	355.4	9.9	11.9	28.0	31.0	124.8	126.4	27.9	-8.1	-68.9	-103.6	34.7	*
		ļ																					
	123	26	4	22		80	13	59	W	170.2	352.5	0.9	20.9	28.0	31.0	104.1	131.3	20.0	-25.0	-56.1	-125.3	69.2	
R	123	26	4	22	N	80	13	59	W	170.2	352.5	0.9	20.9	28.0	31.0	104.1	131.3	21.4	-18.6	-54.7	-118.9	64.2	11
В	104	26		1	N	90	12	10	w	101.0	262.6	5.0	160	20.0	21.0	100.0	1000						1_1
K	124	20	0	6	+14	80	13	19	W	171.7	352.6	5.9	16.0	28.0	31.0	120.3	129.0	20.0	-25.0	-72.3	-122.9	50.7	
R	125	26	1	10	N	80	13	32	w	172.3	352.4	4.6	17.2	28.0	31.0	118.2	129.6	20.0	-25.0	-70.2	-123.6	53.4	┼╌┨
		 - -	 	+	+**	-	1.3	J	+"	174.5	332.7	4.0	17.2	20.0	31.0	110.2	129.0	20.0	-25.0	-70.2	-123.0	33.4	 -
R	126	26	4	27	N	80	14	2	w	172.7	352.4	0.8	21.0	28.0	31.0	103.1	131.4	20.0	-25.0	-55.1	-125.3	70.2	1
R	126	26	4	27	N	80	14	2	W	172.7	352.4	0.8	21.0	28.0	31.0	103.1	131.4	21.4	-18.6	-53.7	-118.9	65.2	1
R	127	26	2	4	N	80	13	44	W	173.4	352.2	3.6	18.3	28.0	31.0	116.0	130.1	20.0	-25.0	-68.0	-124.1	56.1	
		ļ	 	<u> </u>																			Ш
	128	26	1	1		80	13	39	W	174.0	351.9	4.8	17.1	28.0	31.1	118.5	129.5	20.0	-25.0	-70.5	-123.5	53.0	Ц
R	128	26	+	<u> </u>	1 _N	80	13	39	W	174.0	351.9	4.8	17.1	28.0	31.1	118.5	129.5	28.0	-11.0	-62.5	-109.5	47.0	
Q	129	25	59	15	NI	80	13	30	w	174.5	351.4	6.8	15.0	28.0	21 1	121.6	120.4	20.0	36.0	72 (122.4	10 0	
	129	25	59	15		80	13	30	W	174.5		6.8	15.0	28.0	31.1 31.1	121.6 121.6	128.4 128.4	20.0	-25.0 -11.0	-73.6 -65.6	-122.4 -108.4	48.8	
	/	\ 	1-	+:-	+**	-	1-5		+"	1,7.5	351.4		15.0	20.0	74.1	121.0	120.4	20.0	-11.0	ט.נט-	-100.4	72.0	
R	130	26	1	47	N	80	13	48	w	174.9	351.8	3.9	17.9	28.0	31.1	116.7	130.0	20.0	-25.0	-68.7	-123.9	55.2	
	130	26	1	47		80	13	48	W			3.9	17.9	28.0	31.1	116.7	130.0	21.4	-18.6		-117.5	50.2	\Box

Rec.					ve Site											Loss		ceive		ignal	Total	I
Site				Coord	linates				AZ fro			to Tx		RP		Space '		na Gain		evel	<u> 2/U</u>	-
No.		North La				est Lon			"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	Ratio	
	۰	'	"		•	<u> </u>	"		(°)	(°)	mi.	mi.	dBW	dBW	₫B	dB	dB	dB	dB	dB	dB	
	_					J	4							ļ	l	ļ	ļ			<u> </u>		\bot
R 131	25	58	44		80	13	32	W	175.2	350.9	7.4	14.4	28.0	31.1	122.3	128.1	20.0	-25.0	-74.3	-122.0	47.7	┵-
R 131	25	58	44	N	80	13	32	W	175.2	350.9	7.4	14.4	28.0	31.1	122.3	128.1	28.0	-11.0	-66.3	-108.0	41.7	*
				- ,,		1.0		117	100	250 5					100.0	100.	<u> </u>	ļ		1.22.2		<u> </u>
R 132	25	58 58	45		80 80	13	39 39	W	176.1	350.5	7.4	14.5	28.0	31.1	122.3	128.1	20.0	-25.0	-74.3	-122.0	47.8	1-
R 132	25	38	45	- IN	80	13	39	W	176.1	350.5	7.4	14.5	28.0	31.1	122.3	128.1	28.0	-11.0	-66.3	-108.0	41.8	*
R 133	26	1	3	NI	80	14	1	w	178.5	350.7	4.7	17.2	28.0	31.1	118.4	129.6	20.0	-25.0	-70.4	-123.5	53.1	
R 133	26	1	3		80	14	1	W	178.5	350.7	4.7	17.2	28.0	31.1	118.4	129.6	21.4	-18.6	-69.0	-123.3	48.1	+
1.133	20				30	117		- '''	170.5	330.7		17.2	20.0	31.1	110.7	127.0	21.4	-10.0	-09.0	-117.1	40.1	
R 134	25	59	5	N	80	14	25	w	182.4	347.7	7.0	15.0	28.0	31.1	121.8	128.4	20.0	-25.0	-73.8	-122.3	48.5	+
R 134	25	59	5		80	14	25	W	182.4	347.7	7.0	15.0	28.0	31.1	121.8	128.4	31.4	-12.6	-62.4	-109.9	47.5	+-
	1		<u> </u>	1	-			+-										1		10,1,		+-
R 135	25	58	31	N	80	14	38	W	183.9	346.3	7.6	14.4	28.0	31.2	122.6	128.1	20.0	-25.0	-74.6	-121.9	47.3	1
R 135	25	58	31		80	14	38	W	183.9	346.3	7.6	14.4	28.0	31.2	122.6	128.1	31.4	-12.6	-63.2	-109.5	46.3	+1
																						1
R 136	25	58	31	N	80	15	14	W	188.5	343.9	7.7	14.6	28.0	31.2	122.6	128.2	20.0	-25.0	-74.6	-121.9	47.3	\Box
R 136	25	58	31	N	80	15	14	W	188.5	343.9	7.7	14.6	28.0	31.2	122.6	128.2	28.0	-11.0	-66.6	-107.9	41.3	*
															ļ <u>.</u>							
R 137	26	4	32		80	14	15	W	189.6	351.8	0.7	21.1	28.0	31.1	102.0	131.4	20.0	-25.0	-54.0	-125.3	71.3	
R 137	26	4	32	N	80	14	15	W	189.6	351.8	0.7	21.1	28.0	31.1	102.0	131.4	21.4	-18.6	-52.6	-118.9	66.3	\sqcup
D 120	- 05	-	_	- 	00	 		137	101.0	240.0	7.0	115	20.0			1000						
R 138	25 25	58 58	31		80	15 15	41	W	191.9	342.2	7.8	14.7	28.0	31.2	122.7	128.3	20.0	-25.0	-74.7	-122.0	47.3	$\perp \perp$
K 136	_ 23	136	31	IN	80	13	41	W	191.9	342.2	7.8	14.7	28.0	31.2	122.7	128.3	31.4	-11.6	-63.3	-108.6	45.3	\vdash
R 139	26	0	32		80	15	52	w	198.6	344.0	5.6	17.0	28.0	31.2	119.9	129.5	20.0	-24.2	71.0	122.5	50.6	\vdash
R 139	26	0	32	N		15	52	w	198.6	344.0	5.6	17.0	28.0	31.2	119.9	129.5	21.4	-24.2	-71.9 -70.5	-122.5 -116.9	46.4	
	1=0	 •	152	- ``		+==	- -	+**	170.0	311.0	2.0	17.0	20.0	31.2	117.5	129.3	21.4	-10.0	-70.5	-110.9	40.4	
R 140	25	59	13	N	80	16	28	w	199.5	340.3	7.2	15.7	28.0	31.3	122.1	128.8	20.0	-23.5	-74.1	-121.1	47.0	+
R 140	25	59	13		80	16	28	W	199.5	340.3	7.2	15.7	28.0	31.3	122.1	128.8	31.4	-10.6	-62.7	-108.2	45.5	
																						\Box
R 141	26	4	22	N	80	14	27	W	200.0	351.2	1.0	21.0	28.0	31.1	104.5	131.3	20.0	-25.0	-56.5	-125.3	68.7	
R 142	26	1	43		80	15	43	W	202.5	345.6	4.3	18.3	28.0	31.2	117.5	130.1	20.0	-23.9	-69.5	-122.9	53.3	
R 142	26	1	43	N	80	15	43	W	202.5	345.6	4.3	18.3	28.0	31.2	117.5	130.1	28.0	-11.0	-61.5	-109.9	48.4	\square
			<u> </u>	4		1	1	4_4														
R 143	26	0	5		80	18	13	W			7.2	17.3	28.0	31.3	122.0	129.7	20.0	-20.6	-74.0	-119.0	45.0	
R 143	26	0	5	N	80	18	13	W	215.9	335.8	7.2	17.3	28.0	31.3	122.0	129.7	31.4	-10.6	-62.6	-109.0	46.4	
Dist	125			 	00	1.	100	-	010.0	244		10.5			44.5.							
R 144	26	2	42		80	16	25	W		344.4	3.7	19.5	28.0	31.2	116.2	130.7	20.0	-21.3	-68.2	-120.8	52.6	\boldsymbol{oxed}
R 144	26	2	42	$\frac{1}{N}$	80	16	25	W	219.9	344.4	3.7	19.5	28.0	31.2	116.2	130.7	21.4	-18.6	-66.8	-118.1	51.3	
R 145	26	3	3	N7	80	16	7	137	220.3	345 6	2.2	100	28.0	21.2	1140	120.0	20.0	21.5	66.0	121 1	54.2	\dashv
K 143	140	<u> </u> 3	l)	N	JOU	16		w	220.3	J4J.0	3.2	19.9	28.0	31.2	114.9	130.9	20.0	-21.5	-66.9	-121.1	54.2]

R 147 26 1 28 N 80 18 20 W 225.7 337.4 6.1 18.8 28.0 31.3 120.6 130.4 20.0 -19.6 -72.6 -118 R 147 26 1 28 N 80 18 20 W 225.7 337.4 6.1 18.8 28.0 31.3 120.6 130.4 21.4 -18.6 -71.2 -118 R 148 26 0 45 N 80 19 18 W 226.5 333.6 7.4 18.5 28.0 31.3 122.2 130.3 20.0 -19.0 -74.2 -118 R 148 26 0 45 N 80 19 18 W 226.5 333.6 7.4 18.5 28.0 31.3 122.2 130.3 20.0 -19.0 -74.2 -118 R 148 26 0 45 N 80 19 18 W 226.5 333.6 7.4 18.5 28.0 31.3 122.2 130.3 28.0 -14.0 -66.2 -118 R 149 26 1 47 N 80 18 20 W 228.3 337.8 5.8 19.2 28.0 31.3 122.2 130.6 20.0 -19.3 -72.2 -118 R 149 26 1 47 N 80 18 20 W 228.3 337.8 5.8 19.2 28.0 31.3 120.2 130.6 20.0 -19.3 -72.2 -118 R 149 26 1 47 N 80 18 20 W 228.3 337.8 5.8 19.2 28.0 31.3 120.2 130.6 20.0 -19.3 -72.2 -118 R 150 26 3 21 N 80 18 10 W 243.7 340.1 4.7 20.8 28.0 31.3 118.3 131.3 20.0 -16.0 -64.2 -113 R 151 26 3 21 N 80 18 11 W 243.7 340.1 4.7 20.8 28.0 31.3 118.3 131.3 20.0 -16.0 -70.3 -116 R 152 26 4 30 N 80 16 7 W 250.0 346.7 2.2 21.5 28.0 31.2 111.7 131.5 20.0 -16.0 -52.3 -111 R 153 26 2 43 N 80 21 41 W 250.3 330.4 8.3 21.7 28.0 31.2 111.7 131.5 31.4 -10.6 -52.3 -111 R 153 26 5 45 N 80 22 21 W 274.6 333.0 8.5 25.1 28.0 31.3 123.5 132.9 20.0 -16.0 -75.5 -117 R 154 26 5 45 N 80 22 21 W 274.6 333.0 8.5 25.1 28.0 31.3 123.5 132.9 20.0 -16.0 -75.5 -117 R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 123.5 132.9 20.0 -16.0 -75.5 -117 R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 20.0 -16.0 -75.5 -117 R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 20.0 -16.0 -75.7 -118 R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 20.0 -16.0 -75.7 -118 R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 20.0 -16.0 -75.7 -118 R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 20.0 -16.0 -75.7 -118 R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 20.0 -16.0 -75.7 -118 R 155 26 6 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 20.0 -16.0 -75.7 -118 R 155 26 6 6 16 N 80	Total	gnal		eive		Loss											ve Site					Rec.	
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R 147 26	7 46.1	-118.7	-72.6	-19.6	20.0	130.4	120.6	31.3	28.0	18.8	6.1	337.4	225.7	w	20	18	80	N	28	1	26	147	R
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R 152 26 4 30 N 80 16 7 W 250.0 346.7 2.2 21.5 28.0 31.2 111.7 131.5 31.4 -10.6 -52.3 -111 R 153 26 2 43 N 80 21 41 W 250.3 330.4 8.3 21.7 28.0 31.2 123.3 131.6 20.0 -16.0 -75.3 -116 R 153 26 2 43 N 80 21 41 W 250.3 330.4 8.3 21.7 28.0 31.2 123.3 131.6 31.4 -10.6 -63.9 -111 R 154 26 5 45 N 80 22 21 W 274.6 333.0 8.5 25.1 28.0 31.3 123.5 132.9 20.0 -16.0 -75.5 -117 R 154 26 5 45 N 80 22 21 W 274.6 333.0 8.5 25.1 28.0 31.3 123.5 132.9 28.0 -14.0 -67.5 -115 R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 20.0 -16.0 -76.7 -118 R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 28.0 -14.0 -68.7 -116 R 156 26 6 11 N 80 21 49 W 278.5 334.6 8.0 25.3 28.0 31.3 123.5 132.9 133.0 20.0 -16.0 -75.0 -117 R 157 26 6 54 N 80 23 31 W 281.7 332.0 9.9 26.8 28.0 31.3 124.8 133.5 20.0 -16.0 -75.8 -118	6 49.7	-118.6	-68.9	-18.6	21.4	131.3	118.3	31.3	28.0	20.8	4.7	340.1	243.7	W	11	18	80	N	21	3	26	151	R
R 152 26 4 30 N 80 16 7 W 250.0 346.7 2.2 21.5 28.0 31.2 111.7 131.5 31.4 -10.6 -52.3 -111 R 153 26 2 43 N 80 21 41 W 250.3 330.4 8.3 21.7 28.0 31.2 123.3 131.6 20.0 -16.0 -75.3 -116 R 153 26 2 43 N 80 21 41 W 250.3 330.4 8.3 21.7 28.0 31.2 123.3 131.6 31.4 -10.6 -63.9 -111 R 154 26 5 45 N 80 22 21 W 274.6 333.0 8.5 25.1 28.0 31.3 123.5 132.9 20.0 -16.0 -75.5 -117 R 154 26 5 45 N 80 22 21 W 274.6 333.0 8.5 25.1 28.0 31.3 123.5 132.9 28.0 -14.0 -67.5 -115 R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 20.0 -16.0 -76.7 -118 R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 28.0 -14.0 -68.7 -116 R 156 26 6 11 N 80 21 49 W 278.5 334.6 8.0 25.3 28.0 31.3 123.0 133.0 20.0 -16.0 -75.0 -117 R 157 26 6 54 N 80 23 31 W 281.7 332.0 9.9 26.8 28.0 31.3 124.8 133.5 20.0 -16.0 -75.8 -118														$\perp \perp$									
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R 153 26 2 43 N 80 21 41 W 250.3 330.4 8.3 21.7 28.0 31.2 123.3 131.6 31.4 -10.6 -63.9 -111 R 154 26 5 45 N 80 22 21 W 274.6 333.0 8.5 25.1 28.0 31.3 123.5 132.9 20.0 -16.0 -75.5 -117 R 154 26 5 45 N 80 22 21 W 274.6 333.0 8.5 25.1 28.0 31.3 123.5 132.9 28.0 -14.0 -67.5 -115 R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 20.0 -16.0 -76.7 -118 R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 28.0 -14.0 -68.7 -116 R 156 26 6 11 N 80 21 49 W 278.5 334.6 8.0 25.3 28.0 31.3 123.0 133.0 20.0 -16.0 -75.0 -117 R 157 26 6 54 N 80 23 31 W 281.7 332.0 9.9 26.8 28.0 31.3 124.8 133.5 20.0 -16.0 -76.8 -118	4 41.1	116.4	75.2	160	20.0	1216	122.2	21.2	28.0	21.7	9.2	230.4	250.2	11/		21	90		12	12	26	152	- - -
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R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 28.0 -14.0 -68.7 -116 R 156 26 6 11 N 80 21 49 W 278.5 334.6 8.0 25.3 28.0 31.3 123.0 133.0 20.0 -16.0 -75.0 -117 R 157 26 6 54 N 80 23 31 W 281.7 332.0 9.9 26.8 28.0 31.3 124.8 133.5 20.0 -16.0 -76.8 -118		-115.6							28.0	25.1	8.5	333.0	274.6	W						5			
R 155 26 6 16 N 80 23 29 W 277.6 331.3 9.7 26.1 28.0 31.3 124.7 133.2 28.0 -14.0 -68.7 -116 R 156 26 6 11 N 80 21 49 W 278.5 334.6 8.0 25.3 28.0 31.3 123.0 133.0 20.0 -16.0 -75.0 -117 R 157 26 6 54 N 80 23 31 W 281.7 332.0 9.9 26.8 28.0 31.3 124.8 133.5 20.0 -16.0 -76.8 -118																							
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R 157 26 6 54 N 80 23 31 W 281.7 332.0 9.9 26.8 28.0 31.3 124.8 133.5 20.0 -16.0 -76.8 -118	7 47.3	-116.0	-68.7	-14.0	28.0	133.2	124.7	31.3	28.0	26.1	9.7	331.3	277.6	$ \mathbf{w} $	29	23	80	N	16	6	26	155	R
R 157 26 6 54 N 80 23 31 W 281.7 332.0 9.9 26.8 28.0 31.3 124.8 133.5 20.0 -16.0 -76.8 -118	7 42.7 *	1177	75.0	16.0	20.0	122.0	122.0	212	28.0	25.2	- 8 0	2246	278.5	W	40	21	90	- NI	111		26	156	В
	42.1	-11/./	-/3.0	-10.0	20.0	122.0	123.0	31.3	20.0	4.7.3	0.0	337.0	210.3	+*	77	21	100	- 17	1 1		20	120	
	2 41.4 *	-118.2	-76.8	-16.0	20.0	133.5	124,8	31.3	28.0	26.8	9.9	332.0	281.7	w	31	23	80	N	54	6	26	157	R
		-112.8														23				I			
┠╼┾╸┈╽ ╼┈ ╽╸┈┪╸┈┩╸╽┈┈╽╸┈╽┈┈╽╸┈╽╼┈╽┍┈┈┩╸┈╽┈┈╽┈┈╽┈┈╽┈┈╽ ┈┈ ╽╸┈╽																							
┠ ┈╏┈┍╘┈┪═┍╒┈╒┪═╸╒┈┧╶╒╒┉┈┨┈╒ ╇┷╾┉┷┧┈┈ ╒╏┈╒╸╵╿┈ ┩╴┈═╾┱╟┈══╬┼┈╾═╬┈══┈╏┈══┈╸┩┈══┈┼╽┈┈╒┼┈═┈		-117.4																					-
R 158 26 6 17 N 80 19 45 W 282.7 339.2 5.9 24.5 28.0 31.3 120.4 132.7 21.4 -14.1 -71.0 -115.	44.5 *	-115.5	-71.0	-14.1	21.4	132.7	120.4	31.3	28.0	24.5	5.9	339.2	282.7	W	45	19	80	N	17	6	26	158	R
DISC 20 17 17 27 20 10 22 W 292 2 220 7 5 7 24 5 29 0 21 2 120 1 120 7 20 2 120 1 120 7	1 152	1174	72.1	160	20.0	120.0	120.1	21.2	200	24.5	- 5 7	220.7	202.2	1,2,	- 20		00	+	 - - - 	ļ	126	150	
┖╶┍╅╌╌┈┈┧┈┈┈┧╸┈┈┧╸┈┈┧┈┈┈┧┈┈┈┈┼┈┈┈┼┈┈┈ ┼┈┈┈┼┈┈┈┼┈┈┈┼┈┈┈┼┈┈┈		-117.4												_									
R 159 26 6 17 N 80 19 32 W 283.2 339.7 5.7 24.5 28.0 31.3 120.1 132.7 21.4 -15.2 -70.7 -116.	43.9	-116.6	-/0./	-13.2	21.4	134./	120.1	31.3	20.0	24.5	3.1	337./	263.2	 w	32	13	180	12	11/	0	20	139	<u> </u>
R 160 26 7 54 N 80 19 9 W 301.4 341.9 6.1 26.1 28.0 31.3 120.6 133.2 20.0 -16.0 -72.6 -118.	45.4	-118.0	-72.6	-16.0	20.0	133.2	120.6	31.3	28.0	26.1	6.1	341.9	301.4	w	9	19	80	N	54	7	26	160	R
┝╤┉╬┉┉┈┈┧╸╶┈┈╽┈┈┈╶┧╸╽╓┉┈┈┧┈┈┈ ┪┈┈┈┼┈┈┼┈┈┼┈┈┼┈┈┼┈┈┈┼┈┈┈┼┈┈┈┼┈┈┈┼		-116.0																					

1	Rec.				Rece	ive Site										Path	Loss	Rec	eive _	Sig	nal	Total	
	Site				Coor	dinates				AZ fro	om Tx	Dist	to Tx	EI	RP	Free	Space	Antenr	na Gain	Le	vel	D/U	
	No.]]	North La	titude.	$\top \top$	V	Vest Long	itude	T	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	Ratio	
		°	1	"		٥	1	*		(°)	(°)	mi.	mi.	dBW	dBW	dB	dB	dB	dB	dB	dB	dB	
						ļ		ļ.,,															
	161	26	7	47		80	17	1	W	315.5	346.6	4.2	25.4	28.0	31.2	117.5	133.0	20.0	-16.0	-69.5	-117.8	48.4	
R	161	26	7	47	N	80	17	1	W	315.5	346.6	4.2	25.4	28.0	31.2	117.5	133.0	31.4	-5.2	-58.1	-107.0	49.0	
								1	4														
R	162	26	9	3	\perp_{N}	80	17	12	W	324.8	346.9	5.5	26.8	28.0	31.2	119.7	133.5	20.0	-16.0	-71.7	-118.3	46.6	1
		1	-			-		ļ	 	207.0	7.65					1010	100.0		160		1100	45.0	+
	163	26	10	18		80	17	44	W	327.9	346.5	7.0	28.3	28.0	31.2	121.8	133.9	20.0	-16.0	-73.8	-118.8	45.0	1
R	163	26	10	18	\ <u>N</u>	80	17	44	W	327.9	346.5	7.0	28.3	28.0	31.2	121.8	133.9	28.0	-11.0	-65.8	-113.8	48.0	+
	164	26	10	3	- NI	80	17	2	w	332.0	347.8	6.4	27.9	28.0	31.1	121.0	133.8	20.0	-16.0	-73.0	-118.7	45.7	+
	164	26	10	3		80	17	2	W	332.0	347.8	6.4	27.9	28.0	31.1	121.0	133.8	28.0	-10.0	-65.0	-112.7	47.7	+
~	104	20	10	- 3	+"	180	11/	2	- 	332.0	347.0	0.4	21.9	20.0	31.1	121.0	133.6	20.0	-10.0	-03.0	-112.7	47.7	+
R	165	26	9	3	N	80	16	15	W	334.0	349.0	5.0	26.6	28.0	31.1	118.9	133.4	20.0	-13.3	-70.9	-115.5	44.7	+
	100		 	- -	 		 	 	+"	550	315.0	3.0	20.0	20.0	31.1	110.5			13.5	,,,,	1.13.3		+-
R	166	26	9	4	N	80	16	9	w	335.2	349.2	5.0	26.6	28.0	31.1	118.8	133.4	20.0	-13.3	-70.8	-115.5	44.7	+
	166	26	9	4		80	16	9	w	335.2	349.2	5.0	26.6	28.0	31.1	118.8	133.4	21.4	-8.6	-69.4	-110.9	41.5	*
		 			7-		 	 	+										1				+-
R	167	26	11	11	N	80	16	20	W	341.9	349.7	7.3	29.0	28.0	31.1	122.2	134.2	20.0	-2.6	-74.2	-105.7	31.5	*
	167	26	11	11	N	80	16	20	w	341.9	349.7	7.3	29.0	28.0	31.1	122.2	134.2	28.0	-5.0	-66.2	-108.1	41.9	•
					1		1		\top		1				1				<u> </u>		1		
R	168	26	11	7	N	80	16	9	w	343.1	350.1	7.2	28.9	28.0	31.1	122.0	134.1	20.0	-1.8	-74.0	-104.8	30.8	*
													<u> </u>	<u> </u>									
R	169	26	15	35	N	80	17	26	W	344.2	349.4	12.5	34.2	28.0	31.1	126.8	135.6	20.0	-1.0	-78.8	-105.5	26.7	•
R	169	26	15	35	N	80	17	26	W	344.2	349.4	12.5	34.2	28.0	31.1	126.8	135.6	27.9	-2.1	-70.9	-106.6	35.7	•
								1								<u> </u>							
	170	26	13	57		80	16	48	W	344.8	349.9	10.5	32.3	28.0	31.1	125.3	135.1	20.0	-1.0	-77.3	-105.0	27.7	*
R	170	26	13	57	N	80	16	48	W	344.8	349.9	10.5	32.3	28.0	31.1	125.3	135.1	28.0	-5.0	-69.3	-109.0	39.7	*
		<u> </u>			ļ	<u> </u>		ļ			ļ		ļ				L		ļ <u></u>		ļ		!
R	171	26	16	23	N	80	17	27	w	345.2	349.6	13.4	35.1	28.0	31.1	127.4	135.8	20.0	-0.5	-79.4	-105.2	25.8	*
	1.50	1	 	-	+	-	 	 	-	2:22	1	10.5				100.6	107.0	20.0	1 00		1000	05.5	•
K	172	26	16	35	N	80	17	29	W	345.3	349.6	13.6	35.4	28.0	31.1	127.6	135.9	20.0	-0.5	-79.6	-105.3	25.7	+
- D	172	120	10	26	1	80	1.5	26	377	247.0	251.4	- (4	20.2	200	21.1	1210	122.0	20.0	0.1	-73.0	-103.0	29.9	*
	173 173	26 26	10	36 36		80 80	15 15	26 26	W	347.9	351.4 351.4	6.4	28.2 28.2	28.0 28.0	31.1	121.0	133.9 133.9	20.0	-5.0	-65.0	-107.9	42.8	+
-	1/3	20	10	30	11/	100	13	20	- W	347.9	331.4	6.4	20.2	20.0	31.1	121.0	133.9	20.0	-5.0	-03.0	-107.9	72.0	1-1
P	174	26	13	55	N	80	16	11	w	348.1	351.0	10.3	32.1	28.0	31.1	125.2	135.0	20.0	0.0	-77.2	-104.0	26.8	+
	174	26	13	55		80	16	11	w	348.1	351.0	10.3	32.1	28.0	31.1	125.2	135.0	21.4	-8.6	-75.8	-112.6	36.8	+
~		120	1-5	+	17	-	1.5	 ^ ^	+**	J70.1	331.0	10.5	22.1	23.0		123.2	1.55.0		3.0	1	- 12/0	1	+
R	175	26	8	25	N	80	14	41	w	351.4	352.2	3.8	25.6	28.0	31.0	116.5	133.1	20.0	0.0	-68.5	-102.0	33.5	*
R		26	8	25	N		14	41	w		352.2	3.8	25.6	28.0	31.0	116.5	133.1	21.4	-8.6	-67.1	-110.6	43.5	•
		+==	 	120	+ **	-	+	**	+"	331.7	3,2.2	J.0	23.0	23.0	71.0	110.5	1.00.1			† * * * * * *	 	1	+
R	176	26	17	10	N	80	15	53	w	352.6	352.4	13.9	35.8	28.0	31.0	127.8	136.0	20.0	0.0	-79.8	-104.9	25.1	*
	176	26	17	10	N		15	53	w		352.4		35.8	28.0	31.0	127.8	136.0	31.4	-3.6	-68.4	-108.5	40.1	

-	Rec.					ive Sit										Pat	h Loss	R	cceive	5	Signal	' Tota	1
-	Site No.	٠.,	<u> </u>		Coor	dinate					om Tx		t to Tx		EIRP		Space		nna Gain		Level	D/U	
\vdash	No.	- (Vorth La	titude.			West Lo			"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	Ratio	
-	+	+ -	-	 -				"		(°)	(°)	mi.	mi.	dBW	dBW	dB	dB	dB	dB	dB	dB	dB	
F	177	26	17	50	N	80	15	54	W	352.9	352.6	14.7	36.5	20.0	21.0	+							
_	177	26	17	50		80	15	54	w		352.6		36.5 36.5	28.0	31.0	128.2	136.2	20.0	0.0	-80.2		24.9	,
			1	-	+,,	100	1.5	- 34	 ''	332.9	332.0	14.7	36.5	28.0	31.0	128.2	136.2	28.0	-5.0	-72.2	-110.1	37.9	_ [*
	178	26	18	18	N	80	15	58	w	352.9	352.6	15.2	37.1	28.0	31.0	128.6	136.3	20.0	1 00	90.6	1000	1	
R	178	26	18	18	N	80	15	58	W		352.6	15.2	37.1	28.0	31.0	128.6	136.3	28.0	-5.0	-80.6 -72.6	-105.2 -110.2	24.7	
<u> </u>													<u> </u>		1	+ ====	130.5	20.0	-5.0	-/2.0	-110.2	37.7	+
R	179	26	12	58	N	80	15	13	W	352.9	352.5	9.1	30.9	28.0	31.0	124.0	134.7	20.0	0.0	-76.0	-103.7	27.6	
В	180	126	- 			ļ				ļ		,						1	1	70.0	-103.7	27.0	+
R		26 26	14	39 39		80	15	25	W	353.1	352.6	11.0	32.8	28.0	31.0	125.7	135.2	20.0	0.0	-77.7	-104.2	26.5	*
	180	20	14	39	+N	80	15	25	W	353.1	352.6	11.0	32.8	28.0	31.0	125.7	135.2	21.4	-8.6	-76.3	-112.8	36.5	*
R	181	26	8	4	N	80	14	24	W	355.3	352.8	2.4	26.2	200	+	 	ļ						
R		26	8	4		80	14	24	w	355.3	352.8	3.4	25.2 25.2	28.0	31.0	115.4	132.9	20.0	0.0	-67.4	-101.9	34.4	*
			1	T	 }		 • ••	- 	 ''	333.3	332.6	3.7	23.2	20.0	31.0	115.4	132.9	28.0	-5.0	-59.4	-106.9	47.4	<u> </u>
R	182	26	8	41	N	80	14	27	w	355.4	352.9	4.1	25.9	28.0	31.0	117.1	133.2	20.0	0.0	(0)	100.		
	ļ													20.0	31.0	117.1	133.2	20.0	0.0	-69.1	-102.1	33.0	*
<u>R</u>	183	26	9	9	N	80	14	¦25	W	356.4	353.1	4.6	26.4	28.0	31.0	118.2	133.3	20.0	-0.1	-70.2	-102.4	32.3	
	184	26	8	10	-	20			<u> </u>										1	-70.2	-102.4	32.3	Ť
	104	20		10	N	80	14	19	W	356.9	353.0	3.5	25.3	28.0	31.0	115.7	133.0	20.0	-0.1	-67.7	-102.0	34.3	*
R	185	26	14	51	N	80	14	41	w	357.1	354.0	110	22.0	20.0		<u> </u>	ļ						1
	185	26	14	51		80	14	41	W	357.1	354.0	11.2 11.2	33.0 33.0	28.0 28.0	31.0	125.9	135.3	20.0	-0.1	-77.9	-104.3	26.5	*
			1		1		- 	 ''	+"	337.1	334.0	11.2	33.0	28.0	31.0	125.9	135.3	27.9	-2.1	-70.0	-106.3	36.4	*
	186	26	16	5	N	80	14	27	W	358.5	354.6	12.6	34.4	28.0	31.0	126.9	135.6	20.0	0.1	700	10.		<u> </u>
R	186	26	16	5	N	80	14	27	W	358.5	354.6	12.6	34.4	28.0	31.0	126.9	135.6	31.4	-0.1 -3.6	-78.9 -67.5	-104.7	25.8	*
_	105		<u> </u>													120.5	133.0	31.4	-3.0	~07.3	-108.2	40.7	+
	187 187	26	12	28	N		14	20	W	358.6	354.1	8.4	30.2	28.0	31.0	123.4	134.5.	20.0	-0.5	-75.4	-104.0	28.6	*
K	18/	26	12	28	N	80	14	20	W	358.6	354.1	8.4	30.2	28.0	31.0	123.4	134.5	21.4	-8.6	-74.0	-112.1	38.1	*
R	188	26	14	10	N	90	1,4	 	117	250.0	22.1										12211		
	100	20	1-4	- 10	14	80	14	21	W	358.8	354.4	10.4	32.2	28.0	31.0	125.2	135.0	20.0	-0.5	-77.2	-104.6	27.3	*
R	189	26	17	59	N	80	14	14	w	359.6	355.3	14.8	26.5	20.0	21.0								
R	189	26	17	59	N		14	14	w	359.6	355.3	14.8	36.5 36.5	28.0 28.0	31.0	128.3	136.2	20.0	-0.5	-80.3	-105.7	25.4	*
							1	 	+"	222.0	223.3	17.0	20.2	40.U	31.0	128.3	136.2	28.0	-5.0	-72.3	-110.2	37.9	*
_	190	26	7	16	N		9	35	w	62.6	4.3	5.3	24.1	28.0	30.4	119.4	132.6	20.0	-16.0	71.4	110.0	46.5	\square
R	190	26	7	16	N	80	9	35	W	62.6	4.3	5.3	24.1	28.0	30.4	119.4	132.6	27.9	-7.1	-71.4 -63.5	-118.2 -109.3	46.8 45.8	$\vdash \vdash$
_	101	26	1.5	1	1													41.7	-/.1	-0	-103.3	43.8	\vdash
K	191	26	16	15	N	80	17	41	W	344.0	349.2	13.3	35.0	28.0	31.1	127.4	135.8	20.0	-1.0	-79.4	-105.7	26.3	*
p	192	26	 	20	1	00		100	 	245													
	174	20	1	39	N	80	23	29	W	247.4	324.5	10.5	21.6	28.0	31.2	125.3	131.6	20.0	-16.0	-77.3	-116.4	39.1	*
R	193	26	6	11	N	80	17	4	11/	291.4	345.4	2.2	22.6										
				<u> </u>	147	50	11.7	<u> </u>	1 44	471.4	343.4	3.3	23.6	28.0	31.2	115.1	132.4	20.0	-16.0	-67.1	-117.2	50.0	

	Rec.				Recei	ve Site										Path	Loss	Rec	eive	Si	gnal	Total	Ī
	Site				Coore	dinates				AZ fro	m Tx	Dist	to Tx	EI	RP	Free	Space	Anten	na Gain	Le	evel	D/U	
	No.	1	orth Lat	itude.		V	Vest Long	gitude		"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	"D"	"U"	Ratio]
		•		11		۰		"	1	(°)	(°)	mi.	mi.	dBW	dBW	dB	dB	dB	dB	dB	dB	dB	
R	194	26	1	13	N	80	24	26	w	247.0	321.6	11.6	21.8	28.0	31.1	126.2	131.7	20.0	-16.0	-78.2	-116.5	38.4	*
R	194	26	1	13	N	80	24	26	w	247.0	321.6	11.6	21.8	28.0	31.1	126.2	131.7	28.0	-14.0	-70.2	-114.5	44.4	*
R	195	26	7	37	N	80	23	58	w	285.6	331.9	10.5	27.7	28.0	31.3	125.4	133.8	20.0	-16.0	-77.4	-118.5	41.1	*
R	195	26	7	37	N	80	23	58	W	285.6	331.9	10.5	27.7	28.0	31.3	125.4	133.8	28.0	-14.0	-69.4	-116.5	47.1	1
R	196	26	18	39	N	80	11	53	w	8.5	359.1	15.7	37.2	28.0	30.8	128.8	136.3	20.0	-5.0	-80.8	-110.5	29.7	*
R	197	26	1	7	N	80	20	55	w	236.5	329.8	8.4	19.7	28.0	31.2	123.4	130.8	20.0	-16.0	-75.4	-115.6	40.2	*
R	198	26	17	46	N	80	16	53	w	348.9	351.0	14.8	36.6	28.0	31.1	128.3	136.2	20.0	0.0	-80.3	-105.1	24.8	*
R	199	26	1	18	N	80	19	17	w	230.2	334.5	6.9	19.1	28.0	31.3	121.7	130.5	20.0	-18.6	-73.7	-117.8	44.1	*
R	200	26	9	53	N	80	15	15	w	348.0	351.5	5.6	27.4	28.0	31.1_	119.8	133.6	20.0	-0.1	-71.8	-102.7	30.9	*

CERTIFICATE OF SERVICE

I, Kerstin Koops Budlong, hereby certify that on this date I caused the foregoing "Opposition to Petition for Reconsideration" to be served by first class mail, postage prepaid, on the following:

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Kerstin Koops Budlong

Kerstin Koops Budlong

Dated: September 29, 2004